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Bumblebee Program - Aerodynamic

Part III - Pressure Fields at Mach Numbers 1.5 and 2.0

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G. A. Barnes and L. L. Cronvich

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Bumblebee Program - Aerodynamic Data

Part III - Pressure Fields at Mach Numbers 1.5 and 2.0

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Prepared for Langley Research Center under Contract L-60036A



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SUMMARY

This report provides data that supplements the M = 2.0 flow field data given in Part II. The enclosed data package (Appendix A) describes the Mach number effect by means of pressure fields only, at M = 1.5 and 2.0, and at angles of attack up to 23° at a mid-body station where a wing might be located. It was necessary to use the mid-body station for a Mach number comparison since there are no data available from the Bumblebee Program at a Mach number other than 2.0 corresponding to the flow survey station of Part II where a tail surface might be located.

INTRODUCTION

The flow field data given in Part II were compiled for the purpose of aiding the theoretician in his efforts to develop and verify computational methods for defining the complex flow field around missile bodies at relatively high angles of attack. The data of Part II are for M=2.0 and define the flow field around a conical-nosed cylindrical body in a crossflow plane that is a likely location for the tail surface of a missile.

The purpose of this Part III report is to provide additional data that can be used to define the Mach number effect (M = 1.5 and 2.0) on flow field characteristics around a missile body at relatively high angles of attack (to α = 23°).

This report is the third in a four-part series published under the general title:

"Bumblebee Program - Aerodynamic Data"

Part I discusses the purpose of this effort and how the information in the other three reports is related.

Part II presents data at M=2.0 which define the flow field around a conical-nosed, cylindrical missile body in a crossflow plane corresponding to a likely tail location.

Part IV presents wing panel normal force and center of pressure data for three rectangular wings of varying aspect ratio (span) at Mach numbers of 1.5 and 2.0.

NOMENCLATURE FOR TABULATED DATA OF APPENDIX A

p _{t,o} or PTO	free stream stagnation (total) pressure	(in.Hg abs)
$^{p}_{x}$	static or pitot pressure (see Fig. 2) taps 1-6, static; taps 7-15, pitot	(in.Hg abs.)
p _x /p _{t,o}	ratio of a probe pressure (static, p _s , or pitot, p' _t) to free stream total pressure	
Δp/q	ratio of difference between local static and free stream static pressures to free stream dynamic pressure	
Ø or Ø _R	roll attitude of body or rake system; positive is clockwise looking upstream (see Fig. 3 for definition of \emptyset or $\emptyset_R = 0$)	(degrees)
θ	location angle for y or a pitot rake; counterclockwise is positive looking upstream (see Figs. 3 and 4 for definition of $\theta = 0$)	(degrees)
α _i	indicated angle of attack in the vertical plane referred to tunnel centerline; nose up is positive	(degrees)
α _c	$\alpha_{\mathbf{i}}$ corrected for support deflection	(degrees)
у	radial distance from body surface	(inches)

DISCUSSION

Source of Data

The flow field data of Part II provided a complete description of local static and total pressure distributions, local Mach number, and local flow inclination for angles of attack up to 23° at station 3 of the model described in Fig. 1. The M = 2.0 flow field tests (OAL 289-19)* provide data at station 3 for the B₅ body (termed B₁₄ in the wind tunnel test report and in Part II) both alone and in combination with the W₄ wing, and at station 2 for the B₅ body alone as described in Fig. 1. As noted in Part II, the complete flow field tests were conducted at M = 2.0 only.

To describe the Mach number effect, it will be necessary to draw from other tests conducted as part of the overall Generalized Missile Study (GMS) of the Bumblebee Program. During these tests (OAL 289-7, -8, -10, -11, -12)* a limited number of static and pitot pressure data were obtained at M = 1.5 and 2.0 at station (2) (Fig. 1) for the (3) body alone. This station approximates the leading edge of the (4) wing employed in M = 2.0 flow field tests. These static and pitot pressure data and corresponding data from the OAL 289-19 flow field test at M = 2.0 have been reproduced and are presented as Appendix A. The page numbering is identical to that of the OAL reports.

A sketch of the model configuration, locations of the pressure taps on the rake, parameters used to define rake location, and the region of pressure coverage are shown in Figs. 1-4.

The Ordnance Aerophysics Laboratory (OAL) wind tunnel tests from which the Part II and Part III data were obtained are:

Description of Complete Flow Field (Part II)
 OAL Report 289-14, -18, -19, "Survey of the Flow Field Around a Generalized-Missile Model at Mach 2.00," 19 April 1956.

^{2.} Pressure Only (Part III)

OAL Reports 289-7, -8, -10, -11, -12, "Investigation of Induced Roll and Longitudinal Stability Characteristics of a Generalized Missile Model at Mach Numbers of 1.5 and 2.0," 5 and 16 August 1955.

General Comments

Some notes concerning the interpretation of the tabulated pressure data in Appendix A follow.

- Pressures were measured in a plane normal to the body centerline at station \bigcirc on the B₅ body (Fig. 1).
- Data that are not applicable for the purposes of this report have been crossed out.
- The maximum error in the measured pressure coefficients is quoted in OAL wind tunnel data reports as:

$$\Delta p/q = \pm 0.0058$$

 $p_{x}/p_{t_{0}} = \pm 0.0025$

• Certain data sheets for the OAL 289-19, M = 2.0 test are believed to be in error. For the Rake 5 data listings:

$$y = 1.269, 1.469, 1.669, 1.869$$

should read

$$y = 1.069, 1.269, 1.469, 1.669$$

This correction has been made on the data sheets.

- The number 3 static pressure tap (see Fig. 2) for the OAL 289-7,
 -8, -10, M = 2.0 tests was found to be bad after the test data were published; hence, data listed for this tap should be disregarded.
 Data have been crossed out where necessary on the data sheets.
- ullet A general statement is made in the OAL wind tunnel test reports that at high α on the leeward side of the body, some vibration of the pressure probes occurred. This statement implies that the data user should exercise discretion when interpreting data in these areas.
- Table I has been compiled as a data availability matrix for the pressure-only tests (OAL 289-7, -8, -10, -11, -12). The asterisk denotes where more than one run was made for the noted conditions.

As can be seen the matrix is nearly complete at M = 2.0 but not as complete at M = 1.5. However, coverage is complete at α = 20° and 23° at M = 1.5.

For the OAL 289-19, M = 2.0 test, the coverage was as follows:

$$\alpha_{i}$$
 = 0°, 4°, 8°, 12°, 16°, 20° and 23°
$$\emptyset_{R} = \begin{cases} 30^{\circ}, 15^{\circ}, 0^{\circ}, -15^{\circ}, -30^{\circ} \\ -40^{\circ} \text{ through } -135^{\circ} \text{ in } 5^{\circ} \text{ increments} \\ \text{and } -150^{\circ} \end{cases}$$

Data were obtained at each α for all values of ϕ_R .

Refer to Figs. 3 and 4 for a graphic description of location parameters and the region in which data were obtained.

It should be noted that all data given in Appendix A are presented as a function of wind tunnel indicated (or uncorrected) angle of attack, $\alpha_{\rm i}$. Corrected values of angle of attack, $\alpha_{\rm c}$, which include the effect of model support system deflection are given in the following table. These corrected values were obtained from the Stability and Control portions of Generalized Missile Study wind tunnel tests.

αi	α _c (degrees)							
(degrees)	B_5 $M = 1.5$	B_5 $M = 2.0$	$\begin{array}{c} B_5W_4 \\ M = 2.0 \end{array}$					
4	4.1	4.12	4.3					
8	8.2	8.28	8.65					
12	12.3	12.53	13.05					
16	16.6	16.85	17.45					
20	20.9	21.17	21.86					
23	24.1	24.42	25.21					

Examples

In order to assist the user of the data given in Appendix A, the following examples are given.

The following discussion will be concerned with pitot pressure data only since there are considerably more experimental data points giving pitot pressure than giving the static pressure. Also, it is the pitot pressure that would generally be more descriptive in helping to define the character of the flow field.

Since there are pressure data available from two different tests (see Figs. 3 and 4) at M = 2, the first example will be a comparison of these data.

Shown in Fig. 5 for α_i = 20° is p_t^1/p_{t_0} versus distance from the body centerline (y + 0.685 in.) for θ = 90°, 120°, and 150° which, as noted in Fig. 4, is an area where data were obtained with three different pitot pressure rakes. The curves drawn through these points represent an average value of p_t^1/p_{t_0} at any given distance from the body centerline. This single curve representation of the data is probably a good one except possibly in regions of extreme flow activity such as shown in Fig. 5(c), θ = 150°, which, as will be noted subsequently, is in the area of a body vortex.

To exemplify where the plotted data points are given in the tabulated data of Appendix A, refer to Fig. 5(b), $\Theta = 120^{\circ}$, and Figs. 3 and 4.

- 1. Pressure only test, OAL 289-7. The checked data set for $\emptyset = -30^\circ$ on page 550° gives the circles plotted on Fig. 5(b). Taps 7 through 15 apply and p_x stands for p'₁.
- 2. Flow Field test, OAL 289-19.
 Rake 1, $\emptyset_R = 0^\circ$ The checked data sets on pages 233 and 256 set are plotted as the flagged squares in Fig. 5(b).
 Rake 5, $\emptyset_R = -120^\circ$ The checked data sets on pages 328, 351, set and 374 are plotted as the squares in Fig. 5(b). Note that, although data are given to values of y = 3.469, data were not plotted beyond y = 2.069

since that is the extent to which data were available from the pressureonly tests.

The variation of p_t^1/p_{t_0} with Mach number (M = 1.5 and 2.0) at α_i = 20° is exemplified in Fig. 6. The pressure-only tests were used for this comparison.

A typical windward variation is given in Fig. 6(a) for $\theta = 30^{\circ}$. As might be expected, the variation of p_t'/p_t with distance from the body is nearly constant.

A typical leeward variation of p_t'/p_t at θ = 150° is given in Fig. 6(b).

An example of how these pitot pressure data can be used to aid in defining the flow field about the body is given by a comparison of Figs. 5(c), 6(b), and Fig. 7 which made use of Fig. 24 from Ref. 1.

A $\theta=150^\circ$ line and lines of constant distance from the body center-line have been drawn on the total pressure ratio contour of Fig. 7. Note that $H_1/H_0 = p_{t_1}/p_{t_0}$ or local total pressure ratio and not pitot pressure ratio. Refer now to Fig. 5(c) and note that the minimum pitot pressure occurs at a distance of 1.2 inches from the body centerline or as a multiple of the body radius (0.685 inches) at a value of approximately 1.75. Although $\theta=150^\circ$ is not the exact circumferential location of the body vortex, it can be seen that the radial location is approximately 1.75 body radii from the centerline of the body. The data in Fig. 6(b) indicate that the body vortex at M=1.5, $\alpha_1=20^\circ$ may be in the same approximate position as at M=2.0. Additional p_t'/p_{t_0} plots would be required to determine an exact location.

CONCLUDING REMARKS

In summary, this report provides data (specifically pitot pressure ratios) to describe the effect of Mach number (M = 1.5 and 2.0) on the flow field about a body at a mid-body longitudinal station. The existence of significantly reduced pressure regions on the leeward side of a body at high angles of attack (to α = 23°) where a wing may be positioned at certain roll orientations is readily discernible.

REFERENCE

 APL/JHU CM-867, "Investigation of Normal-Force Distributions and Wake Vortex Characteristics of Bodies of Revolution at Supersonic Speeds," J. F. Mello, McDonnell Aircraft Corporation, 2 April 1956.

TABLE I Data Availability Matrix

M = 1.5 and 2.0 (OAL 289-7, -8, -10, -11, -12)

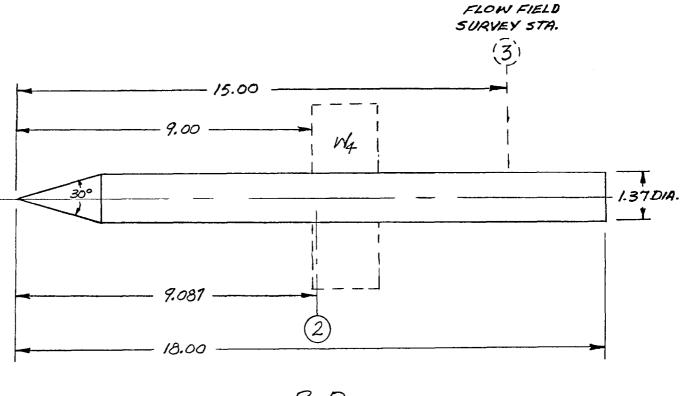
M = 1.5

o°i	90	75	60	45	30	15	0	-15	-30	-35	-40	-45	-50	-55	-60	-65	-70	-75	-80	-90	-105	-120	-135	-150	-165	-180
0							х													Х						Х
4	х	х	х							x	X		x	X		х	x		Х					х	х	X
8	х	х	х							х	X		X	x		х	X		х					x	х	x
12	х	х	x							x	x		х	х		х	x		х					x	x	х
16	x	х	Х							х	X		x	х		X	x		x					x	x	х
20	x	x	x	X	x	х	x	x*	X*	x*	x*	х	х	х	X	х	X	X	х	X	x	x	х	x	х	х
23	х		х	х	X	х	X	х	х	х	X	Х	х	х	x	х	X	X	х	х	X	Х	Х	х	х	х

M = 2.0

a i	•	75	60	45	30	15	0	-15	-30	-35	-40	-45	-50	- 55	-60	-65	-70	- 75	-80	-90	-105	-120	-135	-150	-165	-180
0	х	х	x	Χ¾	х	x	х*	х	х			X*			х					X	X*	x*	х*			
4	х	х	X	x	х	х	X	х	Х	X	X	x	х	х	Χ×	Х	x			x	х	Х	х	х	х	х
8	х	x	х	x	х	x	x	х	х	x	х	х	х	х	χ'n	Х	х			х	х	х	х	x	х	х
12	x	х	X	x	х	x	X	х	x	x	x	x	x ·	x	x*	х	х			х*	х*	X*	х*	x	x	х
16	х	x	X	X	х	x	X	x	x	x	X	x	x	х	х*	х	x			х	х	х	х	x	х	х
20	х	Х	X	x	х	х	х	х	х	х	х	х	х	x	χ*	x	x			x	х	х	х	x	х	х
23	Х	Х	X	х	x	х	Х	х	х	х	х	х	х	x	х*	x	x	х		х	x	х	x	x	x	х

^{*} More than one run



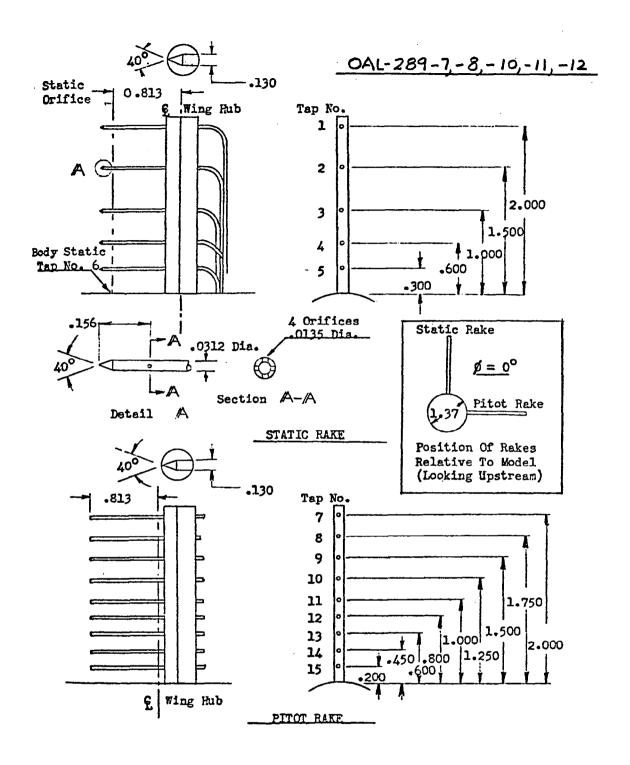
B₅P

NOTES:

11

- 1. STA. 2 LOCATION OF PRESSURE ORIFICES.
- 2. DIMENSIONS IN INCHES.

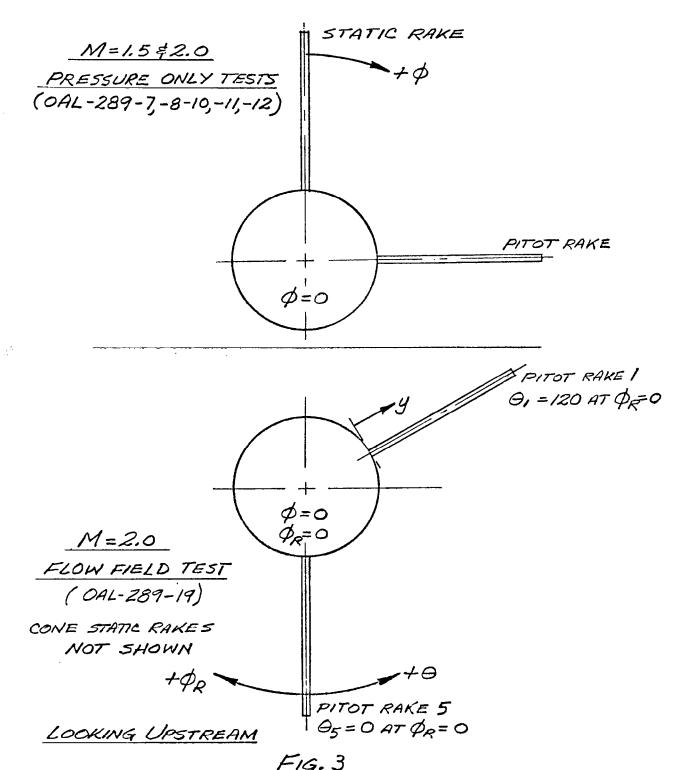
FIG. 1



GENERALIZED MISSILE PRESSURE RAKES

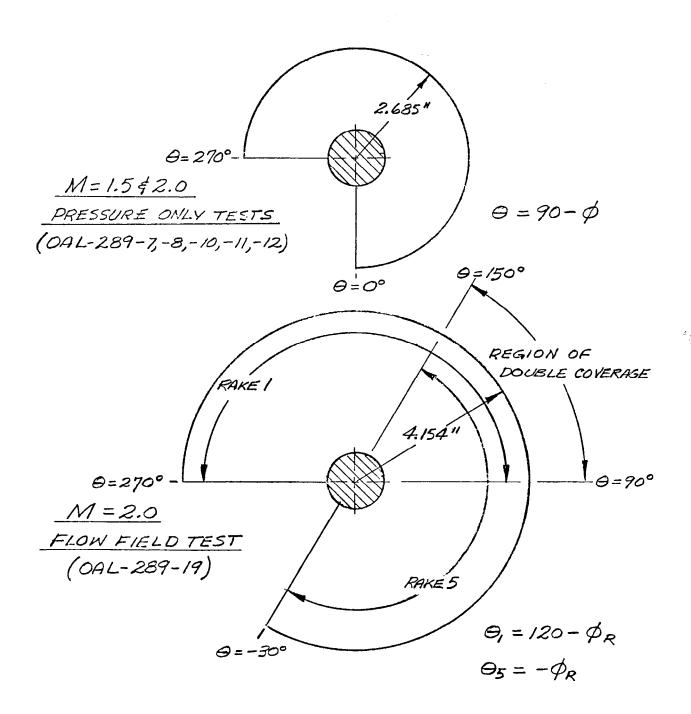
FIG. 2

PRESSURE RAKE ORIENTATION



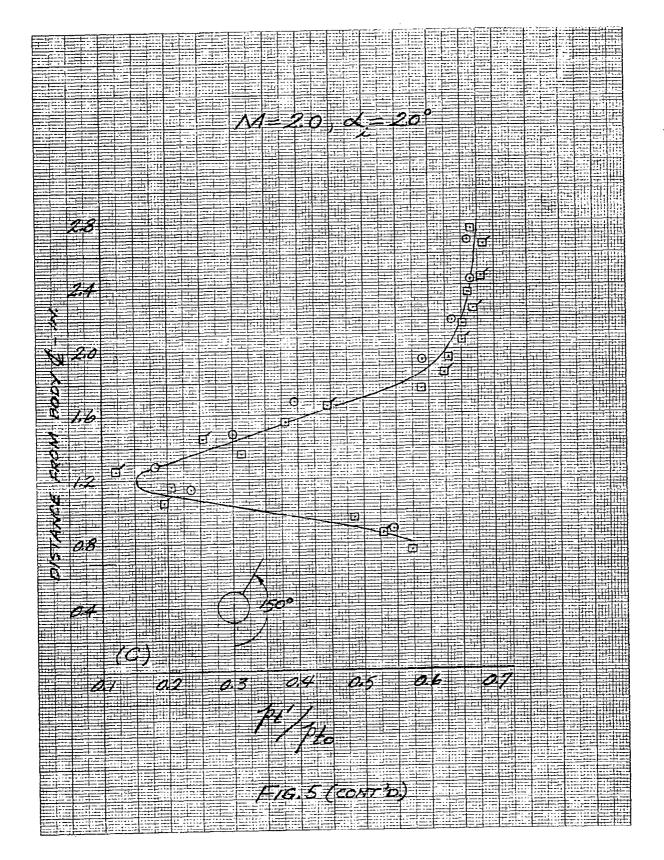
1G. 3

REGION OF PITOT PRESSURE COVERAGE

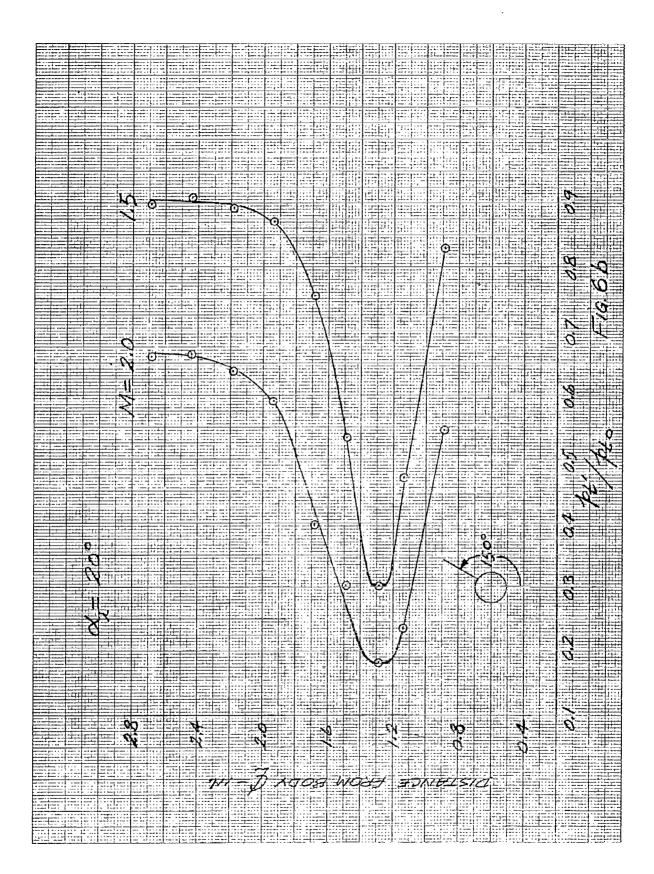


F19.4

		>+		
		PRESSURE C		
	0	RAKE 1 5 20	W FIELD IEST	
28		2,8 0.		7
311				
				9
120 120		1 20		Ø e
2		70 16		
	1 7			b
	70	172		/B
008		0.8		
04		04		
	<i>9=9</i> 0°			
			(2) 3 0.4	
04 (3) 04 (0.7 0 pt/pto	3 0.4	0.5 0.6
		Pt/Ito		
		F16.5		



	PITOT	PRESSUR	E RATIO	
		SURE ONLY		
			7657	
	\sim	(;= 20°		
		7		
	7 2			
287	/= 2.C			
	- O			
24	- o -			
	9	all la la la		
30 20	e	0		
	6	e e		
8 7.6				
	δ	d d		
2 22		0		
		9		
	6			
7 0.8				
0.4				
		6=30		
	7 0.	8 0.9 H/pts	70	
		PE/L		
		/ /°C°		
		- /A+0 F16.6a		
hand from factor for a transfer of the self-self-self-self-self-self-self-self-				
		+16.6U		



EXPERIMENTAL TOTAL PRESSURE RATIO CONTOURS AND LOCAL FLOW INCLINATION $M_{o}=2.00$ $\alpha_{B}\simeq 20^{\circ}$ STATION 2

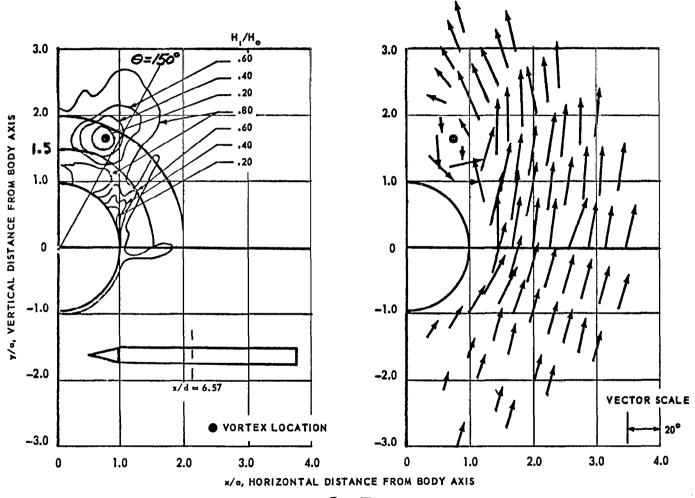


FIG. 7

APPENDIX - A

TABULATED PRESSURE DATA

M = 1.5

OAL 289-11, Runs 2,3,5, Ø = 90 to -180 (pp. 72-109)

M = 2.0

OAL 289-12, Run 15, $\emptyset = 0$ to +90 (pp. $\frac{151-158}{12-88}$) OAL 289-7, Run 27, $\emptyset = +45$ to -45 (pp. $\frac{537-553}{90-109}$)

OAL 289-8, Runs 35, 36, $\emptyset = -60$ to -135 (pp. $5\frac{54}{2}$

OAL 289-10, Run 29, $\phi = -35$ to -180 (pp. $\frac{111-135}{585-606}$)

OAL 289-19, Runs 1,2,3, $\phi_R = +30$ to -150 (pp. $\frac{737^{-7}}{233-397}$ not inclusive, 32 pages in all)

Page numbering from the OAL wind tunnel text reports has been retained.

OAL 289-11

APPENDIX A-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

TAP	Px	<u>Δp</u> q	Ø	$\alpha_{\mathbf{i}}$	Pic	Run	Test
	Pt,o	P		i			
	54.63		000.0	00.	0 1	2	289-11
01	•3676	0.222					
02	•2659	-0.013					
03	• 2632	-0.021					
04	•2632	-0.021					
05	.2669	-0.013					
06	2998	0.064					
0.7	.9240	-					
08	9259						
09	.9295						
10	9277						
11	•9722						
12	9259						
	0259						
	•9259						
15							

APPENDIX A-IV (CONTID) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

```
a, Pic Run Test
PTO 54448
                   -090.0 00.0 2 2 289-11
 01 43631 0.211
 02 -2603 -0-028
 03 -2529 -0-045
 04 +2529 -0+045
 05 .2584 -0.033
 06 .3025 0.070
 07 .9302
 08 .9302
 09 •9321
 10 .9321
 11 •9266
 12 •9321
13 •9302
 14 •9302
 15 •9302
PTO 54.88
                   -180.0 00.0 3 2 289-11
 01 .3595 0.203
 02 42611 -04026
 03 •2593 -0•031
 04 .2593 -0.031
 05 •2684 -0•009
 06 • 2994 0 • 063
 07 49244
 08 .9244
 09 .9244
 10 •9244
 11 49207
 12 •9244
 13 .9244
 14 49244
 15 •9226
                    060.0 04.0 4 2 289-11
PTO 54.68
 01 •3553 0•193
02 •2584 -0•033
 03 +2511 -0+050
 04 .2438 -0.067
 05 •2548 +0•041
06 •2712 -0•003
07 •9223
 08 • 9204
 09 49204
 10 •9223
11 •9223
 12 •9704
 13 •9241
 14 •9241
 15 •9241
```

APPENDIX A-IV (CONTID) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

TAP	Pt.o	<u>op</u> q	ø	a _i F	eic kun	Test
01 02 03 04 05 06 07 08 09 10 11 12 13	•2584 •2474 •2438 •2493		075.0	0440	5 2	289-11
01 02 03 04 05 06 07 08 09 10 11 12 13 14	•2470 •2451	0.180 -0.034 -0.059 -0.064 +0.055 0.039	090.0	04.0	6 2	289-11
PTO 01 02 03 04 05 06 07 08 09 10 11 12 13 14	•2653 •2598 •2653	04193 -04017 -04017 -04029 -04017 -04017	- 035•0	04.0	7 ?	289-11

APPENDIX A-IV (CONT'D) TABULATED PLUSSUKE DALA FOR OAL TEST 289-11 AT MACH HUMBER 1,50

```
TAP Pt.o
                                a, Pic Run Test
PTO 54.58
                      -040.0 04.0 8 2 289-11
  01 •3578 0•199
02 •2552 =0•040
03 •2626 =0•023
  04 -2589 -0-031
 05 •2626 -0.023

06 •2662 -0.014

07 •9276

08 •9276
  09 •9258
  10 •9258
11 •9240
  12 •9240
  13 49258
  14 •9258
  15 .9258
                      -050.0 04.0 9 2 289-11
 PTO 54.48
  01 •3622 0•209
  02 •2557 -0•039
  03 .2557 -0.139
  04 •2594 •0•030
  05 •2594 -0•030
  06 -2722
  07 49275
  08 .9293
  09 49275
  10 •9257
  11 •9238
  12 •9275
  13 +9275
  14 •9275
15 •9275
                       -055.0 04.0 10 2 289-11
 PTO 54.48
  01 •3622 0•209
02 •2557 -0•039
  03 .2539 -0.043
   04 .2557 -0.039
  05 .2575 -0.035
06 .2759 0.008
07 .9275
   08 +9275
   09 .9275
   11 •9238
   12 49293
   13 69275
   14 •9275
   15 .9275
```

APPENDIX A-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

```
Δp
TAP
                             a, Pic Run Test
     Pt.o
  PTO 54.48
                     -065.0 04.0 11 2 289-11
   01 +3640 0.214
   02 +2575 -0+035
   03 #2520 -0.048
   94 +2520 -0+048
   05 -2520 -0-048
   06 .2814 0.021
  07 •9257
08 •9257
09 •9275
   10 •9275
   11 .9275
  12 •9275
13 •9275
  14 •9275
  15 +9275
 PTO 54.43
                     -070.0 04.0 12 2 289-11
  01 •3643 0•214
  02 +2578 -0.034
  03 +2523 -0+047
  04 .2523 -0.047
  05 •2523 -0•047
06 •2835 0•026
  07 •9283
  08 49302
09 49283
  10 .9283
  11 •9283
12 •9283
  13 •9283
  14 •9283
  15 •9265
 PTO 54,43
                    -080.0 04.0 13 2 289-11
  01 •3662 0•219
  02 +2559 -0+038
  03 .2523 -0.047
  04 +2523 -0+047
  05 .2504 -0.051
  06 •2890 0•039
  07 .9302
  08 •9283
  09 .9283
  10 •9283
  11 .9283
  12 .9283
  13 49320
  14 • 9357
  15 •9283
```

APPENDIX A-IV (CONT'D) TABULATED PHESSURE LATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

TAP	Px Pt.o	<u>∆p</u> q	ø	a _i I	Pic Run	Test
01 02 03 04 05 06 07 08 09 10 11	•2532 •2642 •2642 •2660 •3156 •9256 •9256 •9256 •9256 •9256 •9256	0.216 -0.045 -0.019 -0.019 -0.015 0.101	-150.0	04.0	14 ?	289-11
01 02 03 04 05 06 07 08 09 10	.2667 .2630 .2667 .3181 .9238 .9238 .9238 .9238 .9238 .9238 .9238	0.243 -0.017 -0.013 -0.022 -0.013 0.107	-165.0	04.0	15 2	289-11
PTO 01 02 03 04 05 06 07 08 09 10 11 12 13	.7559 .2578 .2559 .2614 .3202 .9210 .9228 .9210 .9228 .9210 .9210	0.227 -0.038 -0.034 -0.038 -0.026 0.111	-180.0	04.0	16 ?	789 - 11

APPENDIX A-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

TAP Pt.o	d <u>7</u> b	ø	a _i I	'ic Ku	n Test
PTO 54.33 01 .3503 02 .2472 03 .2343 04 .2251 05 .2343 06 .2656 07 .9209 08 .9209 09 .9190 10 .9172 11 .9209 12 .9227 13 .9227 14 .9245 15 .9227	-0.059 -0.089 -0.110 -0.089	060•0	08.0	17	? 289 - 11
PTO 54.33 01 .3484 02 .2454 03 .2325 04 .2288 05 .2251 06 .2785 07 .9190 08 .9172 10 .927 11 .9209 11 .9245 12 .927 13 .9264 14 .9264	-0.093 -0.102	075•0	08.0	18	2 289-11
PTO 54.28 01 .3359 02 .2493 . 03 .2308 . 04 .2272 . 05 .2179 . 06 .2824 . 07 .9217 . 08 .9217 . 09 .9217 . 10 .9217 . 11 .9217 . 12 .9162 . 13 .9272 . 14 .9272 .	-0.097 -0.105	090•0	0.80	19	2 289~11

APPENDIX A-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH HUMBER 1,50

```
\Delta P
TAP
   Pt.o
                              a.
                                  Pic Run Test
 PTO 54.33
                     -035.0 0F.0 20 2 289-11
  01 +3558 0+194
  02 •2564 -0•037
03 •2527 -0•046
  04 -2490 -0-055
  05 •2251 =0•110
06 •2601 =0•029
  07 •9301
08 •9282
  09 .9264
  10 .9245
  11 .9227
  12 •9245
  13 .9227
  14 •9227
  15 •9227
 PTO 54.33
                     -040.0 08.0 21 2 289-11
  01 •3595 0•203
  02 .2527 -0.046
  03 42527 -0.046
  04 .2472 -0.059
  05 •2196 -0•123
06 •2601 -0•029
  07 +9282
  08 +9282
  09 •9264
10 •9227
  11 •9227
  12 •9227
13 •9245
  14 •9209
  15 .9227
                     -050.0 08.0 22 2 289-11
 PTO 54.28
  01 •3635 0•212
  02 .2474 -0.058
  03 -2437 -0-067
  04 +2456 -0+062
  05 .2382 -0.080
06 .2622 -0.024
  07 •9272
  08 •9272
  09 .9272
  10 .9235
  11 •9272
  12 •9272
  13 .9272
  14 •9235
  15 .8333
```

APPENDIX A-IV (CONT.) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

```
рx
           \Delta \mathbf{p}
TAP
                           a, Pic Run Test
     Pt.o
                   -055+0 08+0 23 2 289-11
 PTO 54.28
  01 +3653 0+217
  02 -2474 -0.058
  03 .2437 -0.067
  04 .2419 -0.071
  05 +2345 -0+088
  06 .2640 -0.020
  07 •9272
  08 •9272
  09 +9254
  10 49235
  11 •9272
  12 •9272
  13 •9272
  14 .9235
  15 47504
 PTO 54+23
                   -065.0 08.0 24 2 289-11
  01 .3730 0.234
  02 .2476 -0.058
  03 .2421 -0.071
  04 42384 -04079
  05 .2274 -0.105
  06 .2753 0.007
  07 .9299
  08 .9299
  09 .9299
  10 .9281
  11 •9281
  12 •9318
  13 .9299
  14 •9299
  15 .7105
                   -070.0 08.0 25 2 289-11
 PTO 54.33
            0.237
  01 +3742
  02 •2490 -0.055
  03 .2417 -0.072
  04 .2380 -0.080
  05 .2251 -0.110
  06 .2785 0.014
  07 •9301
  08 •9301
  09 49301
  10 •9282
  11 .9282
  12 49301
  13 •9301
  14 .9319
   15 .7736
```

APPENDIX A-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH HUMBER 1.50

TAP I	Px Pt.o	<u>∆p</u> q	ø	a _{j.} Pi	ic Run Test
PTO 01 02 03 04 05 06 07 08 09 10 11 12 13 14 15	•2405 •2387 •2203 •2828 •9301 •9320 •9338 •9356 •9338	0.243 -0.053 -0.074 -0.079 -0.121 0.024	-080.0	08.0	26 2 289-11
PTO 01 02 03 04 05 06 07 08 09 10 11 12 13	.2619 .2674 .3263 .9245 .9227 .9227 .9227 .9245 .9227		-150.0	08.0	27 2 289 - 11
PTO 01 02 03 04 05 06 07 08 09 10 11 12 13 14	•3825 •2555 •2592 •2665	-0.039 -0.031 -0.014 -0.005	~165. 0	08.0	28 2 289-11

APPENDIX A-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

TAP	Px Pt.o	<u>∆p</u> q	ø	α _i 1	Pic Ru	n Test
01 02 03 04 05 06 07 08 09 10 11	.2500 .2518 .2573 .2647 .3033 .9236 .9218 .9199 .9236 .9199 .9199 .9199	0.239 -0.052 -0.048 -0.035 -0.018 0.072	-180.0	08.0	29	? 289 - 11
01 02 03 04 05 06 07 08 09 10 11 12	.2269 .2159 .1938 .1901 .2564 .9209 .9153 .9172 .9117 .9117 .9209 .9227	0.152 -0.106 -0.132 -0.183 -0.192 -0.037	060.0	12.0	30	289-11
PTO 01 02 03 04 05 06 07 08 09 11 12 13 14	•2272 •2161 •2014 •2032	0.165 -0.105 -0.131 -0.165 -0.161 +0.024	075.0	12.0	31 2	289-11

APPENDIX A-IV (CONTID) TABULATED PRESSURE: DATA FOR OAL TEST 289-11 AT RACH NUMBER 1.50

TAP Pt.o	<u>∆p</u> q	ø	a _i Pic R	un Test
03 •2143 04 •2014	0.131 -0.093 -0.135 -0.165 -0.187 -0.050	090•0	12.0 32	2 289-11
03 .2300	0.179 -0.048 -0.099 -0.146 -0.159 -0.030	~ 035•0	12.0 33	? 289 ~11
03 •2309 04 •2107 05 •2217	0.190 -0.062 -0.097 -0.144 -0.118 -0.045	-040.0	12.0 34	? ?89 ~ 11

APPENDIX A-IV (CONT'D) TABULATED PRESSULE DATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

TAP	Pt,o	<u>op</u> q	ø	a _i	Pic	Run	Test
01 02 03 04 05 06 07 08 09 10 11 12	.2083 .1936 .2488 .9218 .9255 .9218	-	 050 • 0	12.0	35	?	289-11
01 02 03 04 05 06 07 08 09 10 11 12	•2288 •2196 •2049 •1846 •2509 •9227	0.212 -0.102 -0.123 -0.157 -0.205 -0.050	-055.0	12.0	36	2	289-11
	•2212 •2047 •1955	-0.098 -0.119 -0.158	- 065•0	12.0	37	7	289-11

APPENDIX A-IV (CONTID) TABULATED PRESSURE TATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

TAP	Pt.o	$\frac{\Delta p}{q}$	ø	a _i	Pic Ru	1 Test
PTC 011 022 03 044 055 067 07 08 011 12 13	.3693 .2313 .2221 .2056 .1927 .2608 .9264 .9301 .9301 .9301 .9320 .9320	0.726 -0.096	-070.0	12.0	38 2	? 289 - 11
10 11 12 13 14 15	•3742 •2306 •2196 •2085 •1865 •2601 •9337 •9337 •9337 •9337 •9337 •9337 •9337 •9337 •9345	0.237 -0.097 -0.123 -0.149 -0.200 -0.029	-080*0	12.0	39 2	289 - 11
01. 02 03		0.255 -0.110 -0.097 -0.050	- 150.0	17.0	40 <i>7</i>	289~11

APPENDIX A-IV (CONT'D) TABULATED PRESSURE DAYA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

<u>∆p</u> q ai Pic Run Test TAP Pt.o -165.0 17.0 41 2 289-11 PTO 54.33 01 43880 0.269 02 .7426 -0.069 03 .2408 -0.074 04 42610 -0±027 05 42702 -04005 06 •3144 0•098 07 •9218 08 •9199 09 •9163 10 •9199 11 .9144 12 •9199 13 •9107 14 .9034 15 .8960 PTO 54,33 -180.0 12.0 42 2 289-11 01 •3742 0•237 02 .2380 -0.080 03 .2343 -0.089 04 .2527 -0.046 05 .2693 -0.007 06 •3135 0•096 07 .9190 08 .9153 09 .9117 10 .9153 11 •9117 12 •9117 13 •9117 14 .9043 15 .8859 PTO 54.33 060.0 16.0 43 2 289-11 01 •3236 0•119 02 •1966 -0•177 03 .1708 -0.237 04 +1542 -0+275 05 .2150 -0.134 06 +2095 -0-147 07 #9273 08 •9218 09 •9255 10 .9163 11 +9218 12 .9199 13 •9236 14 •9255 15 49255

APPENDIX A-IV (CONT'D) TABULATED PHISSURE DATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

```
TAP Pt.o
                              a<sub>i</sub> Pic Run Test
                      075.0 16.0 44 2 289-11
 PTO 54.38
  01 +3233 0+119
  02 .2056 -0.156
  03 •1798 -0•216
  04 •1578 -0 • 267
  05 .1615 -0.758
  06 .2442 -0.066
  07 .9301
08 .9228
  09 •9320
  10 .9246
  11 #9283
  12 •9264
  13 •9320
  14 .9356
  15 •9375
                      090.0 16.0 45 2 289-11
 PTO 54.38
  01 43086 04084
  02 .2166 -0.130
  03 •1890 -0•194
  04 *1762 -0*224
05 *1743 -0*229
   06 .2442 -0.066
  07 .9338
  08 •9301
   09 -9320
   10 .9264
   11 •9301
   12 •9283
   13 •9355
   14 •9393
   15 .9430
                     -035.0 16.0 46 2 289-11
 PTO 54.38
   01 •3380 0•153
   02 .2313 -0.096
   03 *1909 -0*190
   04 •1063 -0•387
05 •1063 -0•387
06 •2313 -0•096
   07 49081
   08 •9172
09 •9081
10 •9044
   11 .8786
   12 $8805
   13 .8455
   14 47278
   15 44961
```

APPHNDIX A-IV (CONT'D) TABULATED PRESSURE DAYA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

```
\nabla \mathbf{p}
                             ai Pic Kun Test
TAP
  PTO 54#38
                      -040.0 15.0 47 2 289-11
   01 +3380 0+153
   02 .2166 -0.130
   03 41762 -04224
   04 -1210 -0-353
   05 .1210 -0.353
   06 +2405 -0+074
   07 .9099
08 .9191
   09 +9117
   10 •9081
   11 +8841
12 +8823
13 +8051
   14 45734
   15 .6764
  PTO 54.38
                     -050.0 16.0 48 2 289-11
   01 •3472 0•174
   02 .2093 -0.147
   03 •1762 -0•224
   04 -1670 -0-246
   05 42056 -0.156
   06 .2258 -0.109
   07 49117
   08 •9209
   09 +9154
   10 +9135
   11 .8915
   12 .8860
   13 #8051
   14 44373
   15 44557
  PTO 54.36
                      -055.0 16.0 49 2 289-11
   01 +3509 0+183
   02 •2056 -0•156
03 •1780 -0•220
   04 .1798 -0.216
   05 •1909 -0•190
06 •2166 -0•130
07 •9172
   08 •9228
   09 •9191
   10 •9154
   11 #9007
   12 +8970
   13 +8345
   14 44961
   15 64741
```

APPENDIX A-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH HUMBER 1,50

M.D	t,o	<u>∆p</u> q	ø	aj. F	Pic Run	Tost
01 02 03 04 05 06 07 08 09 10 11 12 13 14 0	1870 1595 1503	0:199 -0:152 -0:199 -0:263 -0:255 -0:105	- 065•0	16.0	50 2	289-11
01 02 03 04 05 06 07 08 09 10 11 12	•1578 •1523	0.204 +0.143 -0.194 -0.267 +0.280 -0.087	-070 •0	16.0	51 ?	289-11
01 02 03 04 05	•2019 •1688	-0.139 -0.164 -0.241 -0.280 -0.083	-080-0	16.0	52 2	289-11

APPENDIX A-IV (CONT'A) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

```
\mathbf{p}_{\mathbf{x}}
            \Delta \mathbf{p}
                                ai Pic Run Test
TAP
      Pt.o
  PTO 54.38
                       -150.0 16.0 53 2 289-11
   01 •3932 0•282
   02 .2277 -0.104
   03 .2313 -0.096
   04 .2497 -0.053
   05 .2516 -0.048
   06 •3178 0•106
07 •9191
08 •9136
   09 .8989
   10 .9081
   11 +8933
   12 •8933
13 •8823
   14 .8731
   15 •6341
                       -165.0 16.0 54 2 289-11
  PTO 54.38
   01 •4005 0•299
   02 .2424 -0.070
   03 •2460 -0.062
   04 .2681 -0.010
05 .2828 0.024
   06 •3306
              0.136
   07 •9172
   08 .9117
   09 •9025
   10 •9117
   11 •9025
   12 •9044
   13 .8915
   14 +8713
   15 .8529
                       -180.0 16.0 55 2 289-11
  PTO 54.38
   01 43840 0.260
   02 *2424 -0.070
03 *2424 -0.070
   04 •2644 -0.019
    05 •2883 0•037
   06 •3306
07 •9007
              0.136
    08 •9117
    09 .9025
    10 #9117
    11 •9025
12 •9081
    13 49007
    14 #8860
    15 .8639
```

APPENDIX A-IV (CONTID) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH HUBBER 1.50

TAP	Pt,o	<u>∆p</u> q	ø	a _i F	ic kun	Tast
01 02 03 04 05 06 07 08 09 10 11 12	•2568 •2513 •1668 •1750	0.182 -0.036 -0.049 -0.246 -0.225 -0.045	000 • 0	20#0	56 ?	289-11
01 02 03 04 05 06 07 08 09 10 11	.2309 .2199 .1171 .1575 .2272 .8844 .8880 .8935 .8715 .8623 .8807 .8605	0.134 -0.097 -0.122 -0.362 -0.268 -0.105	015.0	20.0	57 2	289-11
PTO 01 02 03 044 05 06 07 08 09 10 11 12 13	•1832 •1300 •1828 •2309 •9082 •9064 •9137 •8954 •8917 •8770 •8605	0.057 -0.208 -0.332 -0.448 -0.302 -0.097	030.0	20•0	58 ?	289-11

APPENDIX A-IV (CONT.D) TABULATED PRESSURE DAYA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

 $\mathbf{p}_{\mathbf{x}}$ <u>∆p</u> a, Pic Run Test TAP Pt.o PTO 54.48 04540 2040 59 2 289-11 01 42805 0.019 02 .1667 -0.246 03 +1391 -0+311 04 •1189 -0.358 05 .1960 -0.178 06 +2199 -0.122 07 +9247 08 +9174 09 •9284 10 .9137 11 •9211 12 •9174 13 •9101 14 .9046 15 .9009 PTO 54.48 060.0 20.0 60 2 289-11 01 •2896 0•040 02 •1648 -0.251 03 41483 -0.289 04 •1465 -0 • 293 05 +2052 -0-157 06 .2144 -0.135 07 .9358 08 •9266 09 •9376 10 +9229 11 .9394 12 49284 13 •9321 14 .9358 15 • 9358 PTO 54448 075.0 20.0 61 2 289-11 01 •2896 0•040 02 •1703 -0•238 03 •1557 -0 • 272 04 +1428 -0+302 05 43557 -04272 06 #2363 -0#079 07 +9394 08 .9302 09 •9431 10 .9339 11 +9431 12 • 9376 13 .9449 14 •9468 15 .9523

APPENDIX A-IV (CONTID) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

TAP Pt.o	<u>∆p</u> q	\$.	a _i F	ic Run	Test
02 •1878 03 •1602 04 •1474 05 •1437	-0.026 +0.197 -0.262 -0.291 -0.300 0.017	090 •0	20.0	62 2	289-11
02	0.138 -0.101 -0.204 -0.444 -0.294 -0.140	-015.0	20.0	1 3	289-11
02 •2000 03 •1339 04 •0771	0.075 -0.169 -0.323 -0.455 -0.289 -0.113	-030.0	20.0	2 3	28911

APPENDIX A-IV (CONT'D) TABULATED PRESSURE DAYA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

```
\Delta \mathbf{p}
TAP
                            a, Pic Hun Test
     Pt.o
 PTO 54.50
                   -035+0 20+0 3 3 289-11
  01 •2991 0•062
  02 •1927 -0 • 186
  03 •1321 -0 • 327
  04 +0935 -0.417
  05 •1670 -0•246
  06 .2275 -0.105
  07 .8716
  08 .8899
  09 .8734
  10 .8606
  11 .8110
  12 .8257
  13 .8239
  14 .7945
  15 .5046
 PTO 54.40
                   -040.0 20.0 4 3 289-11
  01 •2904 0•042
  02 .1783 -0.219
  03 .1342 -0.3?2
  04 -1268 -0-339
  05 •1930 -0•185
  06 .2132 -0.138
  07 •8750
08 •8379
  09 .8732
  10 .8529
  11 • 7849
  12 .7813
  13 .7261
  14 +6544
  15 .5404
                   -015.0 20.0 1 5 289-11
  PTO 54+80
  01 •2245 -0•112
  02 +2354 -0.086
  03 .2080 -0.150
  04 •1040 -0•392
  05 -1551 -0-273
  06 •2190 -0•124
  07 48850
  08 #9015
  09 48887
  10 .8668
  11 .8467
  12 .8577
  13 .8449
  14 .7974
  15 .8412
```

APPENDIX A-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

```
ΔP
                           a, Pic Run Test
PTO 54.90-
                  -030.0 20.0 2 5 289-11
 01 41876 -04198
 02 .2095 -0.147
 03 41366 -0.317
 04 .0765 -0.457
 05 -1475 -0-291
 06 .2240 -0.113
 07 .8743
 08 .8925
 09 .8743
 10 .8670
 11 .8324
 12 .8488
 13 .8434
 14 .7778
 15 45501
                  -035.0 20.0 3 5 289-11
PTO 54.80
 01 •1807 -0•214
02 •2007 -0•167
 03 •1405 -0•307
 04 •0894 +0•427
05 •1588 +0•265
 06 +2245 -0+112
 07 48704
08 •8887
 09 .8704
 10 48595
 11 .8157
 12 .8339
 13 .8266
 14 46423
 15 •4909
                  -040.0 20.0 4 5 289-11
PTO 54.60
 01: +1648 -0 -251
 02 *1850 -0*204
 03 -1502 -0-285
 04 •1190 -0•358
 05 •1832 -0.208
 06 .2179 -0.127
 07 .8718
 08 .8983
 09 .8718
 10 .8535
 11 •7930
 12 #8022
 13 • 7656
 14 .6319
 15 •5110
```

APPENDIX A-IV (CONT'J) TABULATED PRESSURE DAYA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

```
Δp
TAP
                    ø
     Pt.o
             q
                           ai Pic Run Test
 PTO 54460
                   -045.0 20.0 5 5 289-11
  01 +1593 -0.264
  02 +1813 -0.212
  03 .1538 -0.276
  04 •1410 -0.306
  05 +2033 -0.161
  06 •2125 -0 • 140
  07 48773
  08 .8901
  09 .8736
  10 +8516
  11 •7747
  12 • 7546
  13 •6868
  14 •6758
  15 +6117
 PTO 54.60
                   -050.0 20.0 6 5 289-11
  01 -1557 -0-272
  02 •1795 -0.217
  03 •1593 -0 • 264
  04 +1648 -0+251
  05 .2070 -0.152
  06 .2072 -0.152
  07 .8828
08 .8974
  09 .8773
  10 .8590
  11 .7747
  12 .6630
  13 •5879
  14 47051
  15 .8352
 PTO 54.45
                   -055.0 20.0 7 5 289-11
  01 .1543 -0.275
  02 .1763 -0.224
  03 .1616 -0.258
  04 +1781 -0 - 220
  05 +2020 -0+164
  06 .2057 -0.155
  07 .8907
  08 #9035
  09 49834
  10 .8613
  11 .7548
  12 +6428
  13 •4096
  14 .5693
  15 .8430
```

APPENDIX A-IV (CONTID) TABUTATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH HUMBER 1,50

```
\Delta p
                            a, Pic Run Test
                   -060.0 20.0 8 5 289-11
PTO 54.45
 01 .1579 -0.267
 02 .1763 -0.224
 03 +1579 -0.267
 04 +1855 -0,203
 05 .1837 -0.207
 06 .2149 -0.134
 07 .8981
 08 •9091
 09 .8907
 10 48724
 11 .7530
 12 .5326
 13 •3012
 14 44720
 15 .8283
PTO 54.40
                   -065.0 20.0 9 5 289-11
 01 .1581 -0.266
 02 •1765 -0 • 224
 03 •1526 -0•279
04 1857 -0.202
05 1526 -0.279
06 2188 -0.125
 07 +9044
 08 #9154
 09 •9007
 10 .8915
 11 .8107
 12 •5607
 13 •3125
 14 .5129
 15 .8235
PTO 54.30
                   -070a0 20a0. 10. 5 289-11
 01 -1692 -0-262
 02 •1823 -0.210
03 •1547 -0.274
 04 -1713 -0-236
 05 +1602 -0.262
 06 .2247 ~0.111
 07 •9134
08 •9245
 09 •9116
 10 49079
 11 •8729
12 •6722
 13 •4991
 14 .5967
 15 .8250
```

APPENDIX A-IV (CONTED) TABULATED PRESSURY DATA FOR OAL TEST 289-11AT MACH NUMBER 1.50

```
TAP
                             a; Pic Run Test
 P70 54.40
                    -075.0 20.0 11 5 289-11
   01 +1654 -0+249
   02 •1801 -0•215
  03 .1581 -0.266
  04 •1526 -0•279
  05 -1489 -0.288
  06 .2224 -0.117
  07 •9191
  08 +9265
  09 #9210
   10 •9191
   11 •9026
   12 .8732
   13 .7537
   14 .7537
   15 .8254
 PTO 54.45
                    -080.0 20.0 12 5 289-11
  01 •1690 -0.241
  02 •1781 -0•220
  03 .1616 -0.258
  04 •1459 -0•293
  05 •1377 -0 • 314
  06 42167 -0.130
  07 •9201
08 •9275
  09 .9256
  10 .9183
  11 +9128
  12 .8944
  13 .8430
  14 .7952
  15 .8283
 PTO 54.35
                    -090.0 20.0 13 5 289-11
   01 -1472 -0-292
   02 +1895 -0+193
  03 •1766 •0•223
  04 •1527 -0•279
  05 •1288 -0•335
06 •2006 -0•167
  07 •9255
  08 •9292
09 •9255
  10 •9255
  11 •9200
12 •9052
   13 .8548
   14 #8151
   15 .8372
```

APPENDIX A-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH HUMBER 1.50

```
рх
TAP Pt.o
                                 Pic Run Test
                            a4
 PTO 54.35
                    -105.0 20.0 14 5 289-11
  01 •1656 -0•249
  02 •1785 -0•219
  03 +1656 -0.249
  04 .1638 -0.253
  05 •1288 -0 • 335
  06 +1343 -0+322
  07 •9255
08 •9255
  09 •9108
  10 •9181
  11 .8979
  12 .8372
  13 •6127
  14 46845
  15 .8316
 PTO 54.35
                    -120.0 20.0 15 5 289-11
  01 •1711 -0•236
  02 .2098 -0.146
  03 .1858 -0.202
  04 -1914 -0-189
  05 •1417 -0 • 305
  06 .1877 -0.197
  07 .9144
08 .9108
09 .8832
  10 48850
  11 •7912
12 •5833
  13 •3717
  14 44765
  15 .8372
 PTO 54.35
                    -135-0 20-0 16 5 289-11
  01 •1895 -0•193
  02 •2153 ~0•133
  03 .2226 -0.116
  04 •2226 -0•116
  05 •1969 -0•176
05 •2668 -0•013
  07 .8950
  08 .8850
  09 .8556
  10 .8592
  11 .8077
  12 47912
  13 +7470
  14 46569
  15 .5980
```

APPENDIX A-IV (CONT'D) TABULATED PHESSURE DAVA FOR OAL TEST 289-11 AT MACH HUMBER 1.50

```
Px <u>Ap</u>
                               Pic Run Test
TAP
                            \alpha_{4}
     Pt.o
                    -150.0 20.0 17 5 289-11
  PTO 54.30
   01 -2118 -0-141
   02 .2357 -0.086
   03 +2486 -0+055
   04 -2523 -0-047
   05 .2578 -0.034
   06 .3278 0.129
   07 .8969
   09 48600
   10 .8803
   11 .8582
   12 .8656
   13 .8582
   14 .8343
   15 .5341
  PTO 54.30
                    -165.0 20.0 18 5 289-11
   01 .2376 -0.081
   02 .2431 -0.058
   03 +2634 -0+021
   04 +2762 0+009
   05 •3112 0•090
   06 .3333 0.142
   07 49042
   08 +8895
   09 .8656
   10 .8766
   11 .8674
   12 .8729
   13 .8564
   14 *8343
   15 .8269
                     -180.0 20.0 19 5 289-11
   PTO 54.30
   01 -2652 -0.017
    02 .2449 -0.064
    03 .2670 -0.013
    04 .2873 0.035
    05 .3297
06 .3407
              0.134
    07 .8895
    08 .8692
    10 49005
    11 .8877
12 .8603
    13 +8564 14 +8361
    15 47974
```

APPENDIX A-IV (CONTID) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH HUMBER 1.50

```
Pic Hun Test
                            4
PTO 54.30
                     000.0 23.0 20 5 289-11
 01 •2560 •0•038
02 .2634 -0.021
03 -1989 -0-171
04 •1068 -0•386
05 •1694 -0.240
06 42320 -04094
07 .8490
 08 +8656
 09 .8600
 10 .8600
 11 .8361
 12 .8416
 13 .8122
 14 .7422
 15 .7735
PTO 54.30
                    015.0 23.0 21 5 289-11
 01 •2357 -0.086
 02 .2026 -0.163
 03 •1123 -0•373
04 •0681 -0•476
05 •1565 -0•270
 06 .2118 -0.141
 07 48840
 08 •8932
 09 48969
 10 .8729
 11 -8519
 12 .8582
 13 .8250
 14 .7495
 15 .7532
PTO 54.30
                     030.0 23.0 22 5 289-11
 01 .2265 -0.107
 02 •1565 -0•270
03 •1087 -0•382
 04 .0792 -0.450
 05 •1694 +0.240
06 •2265 +0.107
07 •9116
 08 •9116
 09 •9227
 10 49024
 11 •9042
12 •9006
 13 *8821
 14 48343
 15 .8471
```

APPENDIX A-IV (CONT'D) TABULATED PRESSURE DATA FOR GAL TEST 289-11 AT MACH NUMBER 1.50

 $\frac{p_{\chi}}{p_{t,o}}$ $\frac{\Delta p}{q}$ TAP α_{i} Pic Eun Test PTO 54.30 045.0 23.0 23 5 289-11 01 42155 -0.133 02 .1492 -0.287 03 41492 -04287 04 41363 -0.317 05 +1971 -0+175 06 .2026 -0.163 07 .9300 08 •9227 09 +9355 10 .9208 11 •9319 12 •9263 13 .9190 14 •8932 15 •9098 PTO 54.25 060.0 23.0 24 5 289-13 01 .2286 -0.102 02 •1585 +0.265 03 41512 -0.782 04 •1382 -0 • 313 05 •1604 -0.261 06 .2065 -0.154 07 •9419 08 •9309 09 +9456 10 .9364 11 •9493 12 •9438 13 •9419 14 49354 15 •9512 PTO 54.30 090.0 23.0 25 5 289-11 01 .2302 -0.098 02 +1694 -0+240 03 .1621 +0.257 04 •1510 -0.283 05 •1934 -0.184 06 •2320 -0.094 07 .9484 08 49411 09 49558 10 .9484 11 •9595 12 .9521 13 .9535 14 .9669 15 .9687

APPENDIX A-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH HUMBER 1,50

```
<u>Δp</u>
                           ai
                               Pic Run Test
PTO 54.35
                   -015.0 23.0 26 5 289-11
 01 .2079 -0.150
 02 •2153 -0•133
 03 •1086 -0•382
 04 •0644 -0.485
 05 +1546 +0.275
 06 +2098 -0-146
 07 -8629
 08 48850
 09 .8703
 10 .8556
 11 .8169
 12 •8280
13 •8040
 14 47268
 15 .7746
PTO 54.35
                   -030.0 23.0 27 5 289-11
 01 +1656 -0.249
 02 •1877 -0•197
 03 +1030 -0+395
 04 +0828 -0.442
 05 •1564 -0•270
 06 •2171 -0•129
 07 .8408
08 .8666
 09 .8408
 10 .8353
 11 .7930
 12 .8206
 13 .8224
 14 .7672
 15 +5225
PTO 54.35
                   -035.0 23.0 28 5 289-11
 01 •1527 +0•279
 02 •1822 -0•210
03 •1159 -0•365
 04 •1086 -0•382
 05 •1711 -0•236
06 •2079 -0•150
 07 •8335
08 •8574
 09 .8316
 10 •8224
11 •7746
 12 .8077
 13 48151
 14 .7360
 15 +5281
```

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APPENDIX A-IV (CONTED) TABULATED PRESSURE LATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

 $\triangle \mathbf{p}$

Px

a, Pic Run Test TAP q Pt.o -040+0 23+0 29 5 289-11 PTO 54.30 01 •1400 -0•309 02 .1805 -0.214 03 -1308 -0-330 04 41418 -0.304 05 .1842 -0.206 06 •1971 -0•175 07 •8306 08 •8508 09 •8195 10 .8048 11 .7459 12 .7345 13 ,7882 14 -6556 15 45120 -045.0 23.0 30 5 289-11 PTO 54420 01 41365 -0.317 02 -1808 -0-213 03 •1421 -0 • 304 04 -1605 -0-261 05 -1900 -0-192 06 .1919 -0.188 07 .8358 08 +8542 09 48137 10 .7860 11 .7103 12 .7509 13 • 7251 14 +5941 15 •4963 -050.0 23.0 31 5 289-11 PTO 54.35 01 •1325 •0•326 02 •1803 •0•215 03 +1545 -0+275 04 -1674 -0-245 05 +1987 -0-172 06 .1932 -0.185 07 +8445 08 +8629 09 .8151 10 .7599 11 46311 12 •6440 13 .6513 14 47341 15 +6072

APPENDIX A-IV (CONTOD) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH HUMBER 1.50

m.n	t,o	<u>∆P</u> q	ø	a _i F	Pic Run	Test
01 02 03 04 05 06 07 08 09 10 11 12	41786 41621 41805 41897 42026 48564 48729	-0.322 -0.219 -0.257 -0.214 -0.193 -0.163	- 055 _* 0	23.0	32 !	5 289-11
01 02 03 04 05 06 07 08 09 10 11 12	•1805 •1565 •1878 •1694	-0.326 -0.214 -0.270 -0.197 -0.240 -0.146	-060•0	23.0	33 5	5 289 - 11
01 02 03 04 05	•1750 •1473 •1805 •1547	-0.317 -0.227 -0.292 +0.214 -0.274 -0.146	 065 + 0	23.0	34 5	5 289 - 11

APPENDIX A-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

```
TAP
                              a; Pic Hun Test
     Pt.o
  PTO 54.20
                      -070.0 23.0 35 5 289-11
   01 .1384 -0.312
   02 •1753 -0.226
   03 *1458 +0 * 295
   04 .1579 -0.244
   05 •1642 +0•252
   06 42085 -0.149
   07 48948
   08 .9096
   09 .8911
   10 .8450
   11 .5517
   12 •3229
13 •3911
   14 +6107
   15 .8247
  PTO 54.30
                      -075.0 23.0 36 5 289-11
   01 •1418 -0•304
   02 •1768 -0 • 223
   03 •1473 -0•292
   04 •1510 -0.283
05 •1621 -0.257
06 •1952 -0.180
   07 .9061
   09 •9098
   10 .8895
   11 .6667
   12 •5267
   13 •4954
   14 •6777
   15 .8177
  PTO 54.20
                      -080.0 23.0 37 5 289-11
   01 •1273 -0•338
   02 •1790 -0•218
   03 +1494 +0+287
   04 -1476 -0-291
   05 .1587 -0.265
   06 .2011 -0.166
   07 #9151
   08 •9207
09 •9188
10 •9096
11 •8616
   12 47620
   13 +6531
   14 +6605
   15 .8155
```

APPENDIX A-IV (CONT'D) TABULATED PHESSURE DATA FOR OAL TEST 289-11 AT MACH NUMBER 1.50

```
TAP Pt.o
                            a, Pic Kun Test
 PTO 54.25
                    -090+0 23+0 38 5 289-11
  01 •1346 -0•321
  02 •1641 -0 • 252
  03 .1585 -0.265
  04 •1475 -0•291
05 •1475 -0•291
  06 .2120 -0.141
  07 •9235
08 •9272
  09 49235
  10 49180
  11 .8903
  12 .8350
  13 .7041
  14 .6691
  15 .8166
 PTO 54.20
                    -105.0 23.0 39 5 289-11
  01 +1587 -0.265
  02 -1845 -0-205
  03 .1697 -0.239
  04 .1605 -0.261
  C5 +1402 -C+308
  06 +1347 -0.321
  07 •9114
  08 •9133
  09 48948
  10 .8838
  11 +6347
  12 •4705
  13 .4207
  14 .6808
  15 .8173
  PTO 54.15
                    -120.0 23.0 40 5 299-11
  01 +1717 -0+235
  02 +2087 -0+148
  103 41865 -04200
  04 -1921 -0-187
  05 •1551 -0•273
06 •1902 -0•192
07 •8920
   08 .8846
   09 +8292
   10 .7996
   11 .5355
   12 •4783
   13 •4543
   14 .6445
   15 48329
```

APPENDIX A-IV (CONT'D) TABULATED PRESSURE DAYA FOR OAL TEST 289-11 AT MACH HUMBER 1.50

TAP	Px Pt,o	<u>∆p</u> q	ø	a _i Pic l	lun Test
01 02 03 04 05 06 07 08 09 10 11 12	.2306 .2159 .2325 .2048 .2823 .8653 .8487	-0.175 -0.097 -0.132 -0.093 -0.158 0.023	-135.0	23.0 41	5 289 - 11
01 02 03 04 05 06 07 08 09 10 11 12	•2399 •2528 •2675	-0.119 -0.076 -0.046 -0.011	-150.0	23.0 42	5 289-11
01 02 03	.2491	-0.067 -0.054 -0.007 0.062 0.148	-165.0	23.0 43	5 289∞11

APPENDIX A-IV (CONTID) TABULATED PRESSURE DATA FOR OAL TEST 289-11 AT MACH NUMBER 1,50

TAP	Pt,o	<u>∆p</u> q	ø	a _i	Pic R	ın Test
PT0 01	54.20 .2731	0.002	-18040	23.0	44	5 289-11
02		-0.033				
		0.014				
04	•3063	0.079				
05	▶3542	0.191				
06	•3413	0.161				
07	●8856					
0.8	•8616					
09	•8395					
10	•8542					
11	8635					
	8524					
	●8303					
	8044					
15	•4096					

OAL 289-12

APPENDIX B-IV TABULATED PRESSURE DATA FOR OAL TEST 289-12 AT MACH NUMBER 2.00

Tap	p _x	<u>∆p</u>	ø	$a_{\mathbf{i}}$	Pic	Run	Test
PTO 02 03 04 05 06 07 08 09 10 11 12 13 14 15	71.11 .1197 .1197 .1169 .1225 .1239 .6948 .6977 .7019 .7033 .7047	-0.023 -0.023 -0.030 -0.015 -0.011	000•0		1		289-12
	•1162 •1148 •1218 •1232 •7035 •7035 •7049	-0.028 -0.032 -0.036 -0.017 -0.013	060•0	00.0	2	15	289-12
05 06 07 08 09 10	.1148	-0.032 -0.032 -0.036 -0.017 -0.009	075•0	00.0	3	1.5	289-12

APPENDIX R-IV (CONT'D) TABULATED PRESSURE DATA FOR CAL TEST 289-12 AT MACH NUMBER 2.00

Tap	P _x	<u>∆p</u>	ø	α_1	Pic	Run	Test
PTO 02 03 04 05 06 07 08 09 10 11 12 13 14	.1160	-0.033 -0.033 -0.033 -0.014 -0.010	090.00	00.0	4	15	28 9≈1 2
PTO 02 03 04 05 06 07 08 09 10 11 12 13	•7033 •7033 •7033	-0.042 -0.050 -0.058 -0.046 -0.023	090•0	04.0	5	15	289-12
PTO 02 03 04 05 06 07 08 09 10 11 12 13	.1138 .1110 .1068 .1110 .1194 .7018 .7004 .7004 .7018 .7032 .7018 .6990	-0.047 -0.059 -0.047 -0.023	075•0	04.0	6	15	289 - 12

APPENDIX B-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-12 AT MACH NUMBER 2.00

Tap	Px Pt.o	$\frac{\Delta p}{q}$	ø	a _i	Pic	Ru	n Test
PTO	71.31		060.0		7	15	289-12
02		-0.033		U 7 3 U	•	1,5	ZUJ-TE
03		-0.041					
04		-0.057					
05		-0.049					
06	•1242	-0.010					
07	•6992						
0.8	•7020						
09	•7020						
10							
11	•7020						
12	•7020 •6964						
	•6992						
15	6978						
	71.31		060.0	08.0	8	15	289-12
02		~0.057					
03		-0.069					
04 05		-0.088 -0.065					
06		-0.018					
07	•7090	0.010					
	7062						
	•7048						
10							
11	•7006						
12	• 6992						
	•6992						
14	•6978						
15	•6936						
PTO	71.31		075.0	08.0	9	15	289-12
		-0.063					
	•0997	-0.078					
04		-0.098					
05		-0.078					
06		-0.043					
07	•7111						
08 09	▶ 7069						
	●7069 ●7055						
11	•7041						
12							
	•7027						
	•7041						
_	.7027						
	=						

APPEIDIX B-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-12 AT MACH HUNEER 2.00

Tap	P _x	∆p q	ø	α_1	Pic	Run	Test
PTO 02 03 04 05 06 07 08 09 10 11 12 13 14 15	71.31 .1011 .0955 .0913 .0941 .1053 .7125 .7083 .7069 .7055 .7055 .7069 .7069	-0.075 -0.090 -0.102 -0.094 -0.063	0.00	08.40	10	15	289-12
PTO 02 03 04 05 06 07 08 09 10 11 12 13 14 15	71.06 .0832 .0719 .0832 .1043 .7333 .7277 .7249 .7235 .7207 .7249 .7291	-0.125 -0.156 -0.132 -0.125 -0.066	090.0	12.0	11	15	289-12
PTO 02 03 04 05 06 07 08 09 10 11 12 13 14 15	71.31 .0885 .0913 .0759 .0857 .1123 .7322 .7265 .7223 .7209 .7181 .7195 .7223 .7223	-0.110 -0.102 -0.145 -0.118 -0.043	075•0	12.0	12	15	789-12

APPENDIX B-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-12 AT MACH NUMBER 2.00

```
\Delta p
                             a, Pic Run Test
Tap
       pt.o
 PTO 71.36
                     060.0 12.0 13 15 239-12
  02 +0905 -0-104
  03 +0905 -0+104
  04 .0723 -0.155
  05 •0835 -0•124
  06 •1186 -0•026
  07 .7267
  08 •7197
  09 • 7211
  10 .7155
  11 .7127
  12 .7099
  13 •7113
  14 .7099
  15 .7029
 PTO 71.31
                     060.0 16.0 14 15 289-12
  02 .0801 -0.133
  03 •0773 -0•141
  04 .0632 -0.180
  05 •0787 -0•137
  06 .0997 -0.078
  07 *7504
08 •7406
  09 •7476
  10 +7392
  11 .7420
  12 •7364
  13 .7350
  14 .7335
  15 .7237
 PTO 71.21
                    075.0 16.0 15 15 289-12
  02 +0690 -0-164
  03 .0774 -0.141
  04 •0493 -0•219
  05 +0760 -0+145
  06 .0900 -0.106
  07 .7557
  08 .7458
  09 .7500
  10 •7458
11 •7486
  12 .7458
  13 .7472
  14 .7486
  15 .7486
```

APPENDIX B-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-12 AT MACH NUMBER 2.00

Тар	$\frac{p_{x}}{p_{t,o}}$	<u>∆p</u> q	ø	α _i	Pic	Run	Test
PTO 02 03 04 05 06 07 08 09 10 11 12 13	•0690 •0395	-0.145 -0.164 -0.247 -0.133 -0.133	090.0	16.0	16	15	289-12
PTO 02 03 04 05 06 07 08 09 10 11 12 13 14	71.21 .0802 .0861 .0423 .0505 .7851 .77837 .7837 .7839 .7936 .7936 .7950	-0.133 -0.172 -0.239 -0.133 -0.188	090.0	20.0	17	15	289-12
PTO 07 03 04 05 06 07 08 09 10 11 12 13	71.21 .0704 .0605 .0465 .0802 .0774 .7823 .7711 .7823 .7767 .7851 .7837 .7880 .7908 .7823	-0.150 -0.188 -0.227 -0.133 -0.141	075.0	20.0	18	15	289-12

APPENDIX B-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-12 AT MACH HUMBER 2.00

Tap	Px Pt.o	∆p q	ø	a _i	Pic H	un Test
PTO 02 03 04 05 06 07	71.16 .0662 .0676 .0507 .0676 .0831 .7787 .7646	-0.172 -0.168 -0.215 -0.168 -0.125	060•0	20.0	19 1	5 289-12
09 10 11 12 13 14 15	•7773 •7674 •7759 •7730 •7716 •7730 •7520					
PTO 02 03 04 05 06 07 08 09 10 11 12 13 14	71.16 .0690 .0592 .0465 .0690 .0746 .7969 .7929 .8012 .7913 .8026 .7955 .8054 .7829	-0.164 -0.192 -0.227 -0.164 -0.149	060.0	23.0	20 1	5 289-12
PTO 023 034 05 06 07 08 09 10 11 12 13	71.11 .0761 .0578 .0409 .0901 .0719 .8073 .8087 .8017 .8144 .8158 .8270 .8186	-0.144 -0.136 -0.243 -0.105 -0.156	075.0	23.0	21 1	5 289-12

APPENDIK B-IV (CONT'D) TABULATED PRESSURE DATA FOR OAL TEST 289-12 AT MACH NUMBER 2.00

Tap	P _{t,o}	∆p. Q	ø	$\alpha_{\mathbf{i}}$	Pic	Run	Test
PTO	70.96		090.0	23.0	22	15	289-12
0.2	•0875	-0.113					
03	•0692	-0.154					
04	.0466	-0.227					
05	.0889	-0.109					
06	♦0593	-0.191					
07	.B076						
80	•7978						
09	•8090						
10	∙8062						
11	·8175						
12	.8203						
13	8231						
14	8302						
15	.8302						

OAL 289-7

APPENDIX E TABULATED PRESSURE DATA TABLE II OAL TEST 289-7 M = 2.00

TAP	$P_{\mathbf{x}}$	p _x /p _{t,o}	Δp/q	a i	ø	DP	Pic	Run	Test
PTO 1 2	69.55 08.35 08.35	.1201 .1201	-0.022 -0.022	00.0	000	-12	1	27	289-07
4 5 6 7 8 9 10 11 12 13 14	08.35 08.25 08.55 48.55 48.05 48.45 48.75 48.85 48.85 49.05	.1201 .1186 .1229 .6981 .6909 .6966 .7009 .7024 .7024 .7038 .7052	-0.022 -0.026 -0.014						
PTO 1 2	70.10 08.45 08.45	.1205 .1205	-0.020 -0.020	04.0	000	-12	2	27	289-07
4 5 6 7 8 9 10 11 12 13 14 15	08.45 08.45 09.85 48.85 48.35 48.85 49.05 48.95 48.95 48.95 48.85 48.75	.1205 .1205 .1405 .6969 .6897 .6969 .6997 .6983 .6983 .6983	-0.020 -0.020 0.035						
PTO 1 2	70.15 08.05 08.25	.1148 .1176	-0.036 -0.029	08.0	000	-12	3	27	289-07
4 5 6 7 8 9 10 11 12 13 14	08.65 08.65 09.05 48.25 47.85 48.25 48.35 48.25 48.25 47.65 47.55 46.95	.1233 .1233 .1290 .6878 .6878 .6878 .6878 .6878 .6793 .6778 .6693	-0.013 -0.013 0.003						

```
TAP
             p_x/p_{t,0} \Delta p/q
      \mathbf{p}_{\mathbf{x}}
                                    DP Fic Run Test
                           G.
PTO 70.35
                           12.0 000 -12 4 27 289-07
  1 07.65 .1087 -0.053
  2 07.95 .1130 -0.041
  4 08.65 .1230 -0.013
  5 08.65 .1230 -0.013
  6 09.05 .1286 0.002
  7 47.05 .6816
  8 47.35 .6731
  9 47.35 .6731
 10 46.45 .6603
 11 45.45 .6461
 12 44.95 .6389
 13 46.05 .6546
 14 46.95 .6674
 15 46.25 .6574
PTO 70.65
                          16.0 000 -17 5 27 289-07
  1 06.95 .0984 -0.082
  2 07.75 .1097 -0.051
  4 07.75 .1097 -0.051
  5 06.45 .0913 -0.102
  6 07.15 .1012 -0.074
  7 47.75 .6759
  8 47.25 .6688
  9 47.25 .6638
 10 45.95 .6504
 11 44.45 .6292
 12 42.85 .6207
 13 42.05 .5052
 14 42.65 .6037
 15 42.15 .5965
PTO 69.65
                          20.0 000 -17 6 27 280-07
  1 06.60 .0948 -0.002
  2 97.99 .1134 -0.040
  4 02.70 .0388 -0.249
  5 03.80 .0546 -0.205
  6 05.60 .0804 -0.132
  7 47.70 .6849
  8 47.40 .6905
 9 47.40 .6805
10 45.90 .6590
31 43.80 .6289
 12 43.40 .5231
13 41.20 .5015
14 38.00 .5455
 15 33.90 .4867
```

```
TAP
            p_x/p_{t,o} \Delta p/q
     Px
                           OF A
                                   DP Pic Run Test
                           23.0 000 -17 7 27 289-07
PTO 69.40
  1 06.80 .0980 -0.083
  2 08.30 .1196 -0.023
  4 01.60 .0231 -0.293
  5 03.60 .0519 -0.212
  6 05.10 .0735 -0.152
  7 48.60 .7003
  8 48.10 .6931
  9 47.80 .6888
 10 46.40 .6586
 11 44.10 .5354
 12 43.50 .6268
 13 41.60 .5994
 14 38.20 .5504
 15 33.50 .4827
PTO 70.05
                          00.0, 015 -18 3 27 299-07
  1 08.40 .1199 -0.022
  2 08.30 .1185 -0.026
  4 08-30 -1185 -0-026
  5 08.20 .1171 -0.030
  6 08.40 .1199 -0.022
7 48.40 .5909
  5 48.70 .5952
 9 49.00 .6905
10 49.20 .7024
 11 49.40 .7052
 12 49.40 .7052
 13 49.40 .7052
 14 49.40 .7052
 15 49.50 .7066
PTO 69.35
                          04.0 015 -18 9 27 289-07
  1 08.40 .1211 -0.110
2 08.30 .1197 -0.023
  4 08.30 .1197 -0.023
  5 03.20 .1182 -0.027
  5 09.60 .1384 .0.030
  7 47.70 .6278
  8 48.10 .6936
 9 48,40 .6979
 10 48.50 .6994
 11 48.50 .6994
 12 48.40 .6979
 13 47.20 .6806
 14 45,40 .6979
15 48.30 .6965
```

```
TAP
            p_x/p_{t,o}^{\Delta p/q}
                                   DP Pic Rum Test
                           \alpha_{\mathbf{z}}
      \mathbf{p}_{\mathbf{x}}
PTO 69.65
                           08.0 015 -18 10 27 289-07
  1 08.10 .1163 -0.032
   2 08.00 .1149 -0.036
  4 08.30 .1192 -0.024
   5 08.20 .1177 -0.028
  6 09.20 .1321 0.012
  7 47.50 .6820
  8 47.50 .5853
  9 48.00 .6892
 10 47.90 .6877
 11 47.60 .6834
 12 47.60 .6834
 13 47.00 .6748
 14 47.10 .6762
 15 46 50 6576
                           12.0 015 -18 11 27 239-07
PTO 69.65
   1 07.40 .1062 -0.060
   2 07.50 .1077 -0.056
  4 07.90 .1134 -0.040
   5 08.00 .1149 -0.036
  6 Q8.60 .1235 -0.012
7 47.40 .6805
  8 47.60 .6834
  9 47.70 .6849
 10 47.10 .6762
 11 45.30 .6648
 12 45.90 .6590
 13 44.60 .5403
 14 43,00 .6289
 15 41.,50 .5958
PTO 70.00
                           16.0 015 -18 12 27 280-07
   1 06.30 .0971 -0.035
   2 07.00 .1000 -0.078
  4 05.70 .0814 -0.130
   5 04.30 .0685 -0.165
  6 76.20 .9886 -7.110
  7 48.60 .6943
  8 48.70 .6957
  9 48.80 .5971
 10 47.80 .6829
 11 46.80 .6686
 12 45.30 .6614
 13 45.20 .6457
 14 43.40 .6200
 15 40.60 .5800
```

```
p_x/p_{t,o} \triangle p/q
                                   DP Pic Run Test
TAP
                           a,
      \mathbf{P}_{\mathbf{x}}
                           20.0 015 -18 13 27 289-07
PTO 69.80
   1 06.20 .0888 -0.109
   2 06.40 .0917 -0.101
  6 01.80 .0250 -0.235
  5 03.90 .0544 -0.205
   6 05.60 .0802 -0.133
   7 50.00 .7163
  8 49.90 .7149
  9 50.20 .7102
 10 49.00 .7020
 11 47.10 .6862
 12 47.60 .6819
 13 46.10 .5605
 14 43.70 .5261
 15 40.50 .5802
PTO 69.85
                          23.0 015 -10 14 27 289-07
  1 06.00 .0859 -0.117
  2 05.60 .0802 -0.133
  4 01.40 .0200 -0.301
  5 03.50 .0501 -0.217
  6 05.00 .0716 -0.157
  7 51.20 .7330
  8 51.20 .7330
  9 51.60 .7387
 10 50.30 .7201
 11 49.10 .7029
 12 49.00 .7015
 13 47.40 .6796
 14 45.00 .6442
 15 41.20 .5898
PTC 69.85
                          00•0 030 +18.15 27 289+07
  1 08.50 .1217 -0.017
2 08.40 .1203 -0.021
  4 08.30 .1188 -0.025
  5 08.10 .1160 -0.033
  6 08.40 .1203 -0.021
  7 48.90 .7001
  8 49.20 .7044
  9 49.20 .7044
 10 49.30 .7058
 11 49.40 .7072
 12 49.30 .7058
 13 49.30 .7058
 14 49.49 .7072
 15 49.40 .7072
```

```
p_x/p_{t,o}^{\Delta}p/q
TAP
                                  DP Pic Rum Test
      Px
PTO 69.85
                          04.0 030 -18 16 27 289-07
   1 03.50 .1217 -0.017
  2 08.30 .1188 -0.025
  4 08.20 .1174 -0.029
  5 08.10 .1160 -0.033
   5 09.50 .1374 10.027
  7 48.90 .7001
  8 49.10 .7029
  9 49.10 .7029
  10 49.20 .7044
  11 40.10 .7020
  12 49.00 .7015
  13 48.10 .6836
 14 48.80 .6986
  15 48.60 .6958
PTO 59.75
                          08.0 020 -18 17 27 280-07
  1 08.10 .1161 -0.033
   2 07.80 .1118 -0.045
  4 07.70 .1104 -2.049
  5 07.10 .1018 -0.073
  6 08.90 .1276 -0.001
   7 48.70 .5932
  8 48.70 .6982
  . 9 48•70 •6992
10 43•40 •6939
  11 48.20 .6910
  12 48.00 .6382
  13 47.60 .65?4
  14 47.30 .6781
  15 46.70 .6695
                          12.0 030 -13 18 27 289-07
PTC 69.75
   1 07.40 .1061 ₩0.061
   2 07.20 .1032 -0.059
  4.06.30 .0903 -0.105
   5 04.70 .0674 -0.169
  6 05.00 .0717 -0.157
  7 49.30 .7050
  8 49.20 .7054
  9 49.00 .7025
  10 48.40 .6939
  11 48.00 .6882
  12 47.70 .6839
  13 47.00 .6738
  14 46440 • 5557
  15 45.10 .6466
```

```
p_{x}/p_{t,o}\Delta p/q
TAP
                                     Ø DP Pic Run Test
      \mathbf{p}_{\mathbf{x}}
                           \alpha_{g}
PTO 70.05
                            16.0 030 -18 19 27 289-07
   1 06.50 .0928 -0.098
   2 06.00 .0857 -0.118
   4 01.80 .0257 -0.285
   5 03-10 -0443 -0-233
   6 06.40 .0914 -0.172
   7 50.50 .7209
  8 50.50 .7209
  9 50.50 .7223
 10 49.80 .7109
 11 49.30 .7038
12 48.90 .6981
 13 47.40 .5767
 14 47.10 .6724
 15 45.50 .6510
PTO 69.05
                           20.0 -330 -18 20 27 289-07
  1 05.90 .0845 -0.121
  2 04.90 .0702 -0.161
  4 01.70 .0243 -0.289
  5 04.20 .0601 -0.189
  6 06.00 .0859 -0.117
  7 52.10 .7459
  8 52.00 .7445
  9 52.40 .7502
 10 51.60 .7387
 11 51.20 .7330
 12 50.90 .7287
 13 50.00 .7158
 14 48 460 46958
 15 46.20 .6614
PTO 69.75
                           23.0 030 -18 21 27 289-07
  1 05.20 .0745 -0.149
2 04.40 .0631 -0.181
  4 01.60 .0220 -0.203
  5 03.50 .0502 -0.217
  6 05.50 .0783 -0.137
  7 53.30 .7542
  3 53,40 .7556
 0 53.00 .7728
 10 52.90 .7584
 11 53.70 .7556
 12 52.60 .7541
13 51.70 .7412
 14 50.30 .7211
15 47.80 .6853
```

```
p_x/p_{t,o}^{\Delta p/q}
                           a.
                                   P Pic Run Test
TAP
      \mathbf{p}_{\mathbf{x}}
                           00.0 045 -18 22 27 289-07 -
PTO 69.75
  1 08.50 .1219 -0.016
   2 08.30 .1190 -0.025
   4 08.20 .1175 -0.029
  5 08.10 .1161 -0.033
6 09.40 .T204 -0.02T
  7 49.30 .7068
  8 40.10 .7030
  9 49.20 .7054
 10 49.20 .7054
  11 49.30 .7068
 12 49.30 .7068
 13 49.40 .7092
 14 49.40 .7027
  15 49 40 .7082
                           04.0 045 -18 23 27 289-07
 PTO 59.65
   1 08.50 .1220 -0.016
   2 08.30 .1192 -0.024
   4 08.10 .1163 -0.032
  5 08.00 .1149 -0.036
  6 09.20 .1321 0.012
  7 48.90 .7021
  8 48.90 .7021
  9 48,90 .7021
  10 48.90 .7021
  11 48.90 .7021
  12 48.90 .7006
  13 48.20 .5920
  14 48.60 .5978
  15 48.50 .6963
                           08.0 045 -18 24 27 289-07
 PTO 69.40
   1 08.00 .1153 -1.035
   2 07.60 .1095 -0.051
   4 07.20 .1037 -0.067
   5 06.80 .0980 -0.083
   6 08.40 .1210 -0.019
   7 40.10 .7075
   8 40.00 .7061
   9 48.80 .7032
  10 48.50 .7003
  11 48.60 .7003
  12 48.40 .6974
  13 48.20 .6945
  14 47.80 .6888
  15 47.40 .6830
```

```
p_x/p_{t,o} \Delta p/q
TAP
                                   Ø DP Pic Rum Test
                           a:
      p_{\mathbf{x}}
PTO 69.50
                           12.0 045 -18 25 27 289-07
  1 07.30 .1050 -0.064
   2 06.50 .0935 -0.096
   4 05.10 .0734 -1.152
   5 04.00 .0691 -0.164
  6 06.30 .0906 -0.104
   7 50.30 .7237
  8 50.00 .7194
  9 49.00 .7180
 10 49,40 .7108
 11 49.20 .7079
 12 48.90 .7036
 13 48.60 .699?
 14 48 20 6935
 15 47.60 .5849
PTO 69.65
                          16.0 045 -18 26 27 289-07
  1 06.35 .0912 -0.102
  2 05.45 .0782 -0.139
  4 04.05 .0581 -0.195
  5 05.35 .0768 -0.143
  6 06.95 .0998 -0.078
7 51.85 .7444
  8 51.35 .7373
 9 51.55 .7401
10 50.85 .7301
 11 50.35 .7301
 12 50 55 7258
 13 49.65 .7102
 14 49.55 .7114
 15 48.95 .7028
PTO 59.65
                          20.0 045 -18 27 27 289-07
  1 05.75 .0826 -0.126
  2 04.95 .0711 -0.158
  4 04.45 .0639 -0.179
  5 05.25 .0754 -0.146
  6 05.45 .0926 -0.098
  7 53.45 .7674
  8 53.75 .7617
  9 53.55 .7588
 10 52.95 .7502
 11 53.15 .7531
 12 52.95 .7602
 13 52.55 .7545
 14 51.95 .7459
 15 50.55 .7258
```

```
p_x/p_{t,o}^{\Delta_p/q}
                           a.
                                   p DP Pic Run Test
TAP
      \mathbf{p}_{\mathbf{x}}
PTO 69.40
                           23.0 045 -18 28 27 280-07
  1 05.15 .0742 -0.150
   2 05.15 .0742 -0.150
  4 04.25 .0612 -0.186
   5 04.95 .0713 -0.158
   6 05.75 .0829 -0.125
  7 54.75 .7889
  3 54.45 .7846
  9 55.15 .7947
 10 54.45 .7846
 11 54.75 .7889
 12 54.75 .7889
 13 54.35 .7831
 14 53.85 .7759
 15 52.55 .7572
                          00.0 -015 -18 29 27 289-07
PTO 69.55
  1 08.50 .1237 -0.011
  2 08.40 .1208 -0.020
  4 08.40 .1203 -0.020
  5 08.30 √1193 ~0.024
  6 08.60 .1237 -0.011
  7 48.50 .6973
  8 48.50 .6973
 . 9 48.80 .7017
 10 49.00 .7045
 11 49.10 .7060
 12 49.10 .7060
 13 49.00 .7045
 14 49.10 .7060
 15 49.20 .7074
PTO 69.80
                          04.0 -015 -18 30 27 289-07
  1 08.60 .1232 -0.013
2 08.50 .1218 -0.017
  4.08.50 .1218 -0.017
  5 08.50 .1219 -0.017
  6 09.90 .1418 0.039
  7 49.10 .7034
  9 49.00 .7020
  9 49,40 .7077
 10 49.30 .7049
 11 49.20 .7049
 12 49.10 .7034
 13 49.10 .7034
 14 49400 .7020
 15 48.70 .6977
```

```
px/pt,o Ap/q
TAP
       p<sub>x</sub>
                             \alpha_{\vec{k}}
                                       Ø DP Pic Run Test
 PTO 69.95
                             08.0 -015 -18 31 27 289-07
   1 08.30 .1187 -0.025
   2 03.30 .1187 -0.025
   4 08.50 .1215 -0.019
   5 08.20 .1172 -0.030
6 09.60 .1372 0.025
   7 48.80 .6976
   3 48.70 .6962
9 49.20 .7034
  10 49.10 .7019
 11 49.00 .7005
12 48.90 .6991
 13 48.70 .6962
 14 48.20 .6891
 15 47.80 .6833
PTO 69.90
                             12.0 -015 -18 32 27 289-07
  1 07.80 .1116 -0.045
  2 08.00 .1144 -0.037
  4 08.20 .1173 -0.029
  5 07.80 .1116 -0.045
  6 09.70 .1245 -0.009
  7 47.40 .6791
  8 45.90 .6710
 9 48.30 .6910
 10 49.50 .6939
 11 47.70 .6824
 12 47.90 .6653
 13 47.60 .6010
 14 46.50 .5667
 15 45 80 .6552
PTO 69.90
                            16.0 -015 -18 33 27 299-07
  1 07.20 .1030 -0.069
2 07.60 .1087 -0.053
  4 05.30 .0758 -0.145 5 04.20 .0501 -0.180
  6 06.20 .0287 -0.109
  7 46.10 .6595
  8 45.70 .55311
 9 45.40 .6495
10 43.80 .5265
11 45,20 .6466
12 45.50 .6509
12 44.10 .5309
14 41.30 .5990
15 41.00 .5866
```

```
p_x/p_{t,o} \Delta p/q
TAP
                                   DP Pic Run Test
                           a.
      \mathbf{p}_{\mathbf{x}}
PTO 69.90
                           20.0 -015 -18 34 27 289-07
   1 06.60 .0944 -0.093
   2 07.00 .1001 -0.077
   4 01.50 .0215 -0.297
   5 03.70 .0529 -0.209 6 05.60 .0801 -0.133
  7 44.90 .6423
  8 44.80 .6409
  9 44.10 .6309
  10 42.40 .6066
  11 39.30 .5622
 12 41.30 .5008
 13 40,40 .5730
 14 38.60 .5522
 15 38.00 .5436
PTO 69.80
                           27.0 -015 -18 35 27 289-07
   1 05.20 .0889 -0.109
   2 06.80 .0974 -0.085
  & 01.40 .0201 -0.301
   5 03.20 .0458 -0.229
   6 05.10 .0731 -0.153
  7 45.10 .6461
  8 45.00 .6447
  9 43.80 .6275
 10 42.20 .6046
 11 38.60 .5530
 12 38.50 .5516
 13 36.50 .5244
 14 37.20 .5330
 15 35.80 .5129
PTO 69.80
                           00.0 -130 -18 36 27 289-07
  1 08.60 .1232 -0.013
  2 08.40 .1203 -0.021
  4 08.40 .1203 -0.021
  5 08.30 .1189 -0.025
  6 08.60 .1232 -0.013
  7 49.10 .7034
  8 49.40 .7077
  9 49450 47092
 10 49.60 .7106
 11 49.50 .7092
 12 49.30 .7063
 13 49.20 .7049
 14 49.30 .7063
 15 49.30 .7063
```

```
p_x/p_{t,o} \Delta p/q
TAP
                           \alpha_{\vec{a}}
                                    Ø DP Pic Run Test
      \mathbf{p}_{\mathbf{x}}
                           04.0 -030 -18 37 27 289-17
PTO 69.80
  1 08.50 .1218 -0.017
  2 08.50 .1218 -0.017
  4 08.40 .1203 -0.021
  5 08.30 .1189 -0.028
  6 09.60 .1375 0.027
  7 49.50 .7092
  8 49.60 .7105
  9 49.90 .7135
 10 49.70 .7120
 11 49.60 .7106
 12 49.60 .7106
 13 49450 .7092
 14 49.20 .7049
 15 49.00 .7030
                           08.0 -130 -18 38 27 289-07
PTO 69.80
  1 08.10 .1160 -0.033
  2 08.20 .1175 -0.029
  4 07.90 .1132 -0.041
  5 07.20 .1032 -0.069
  6 09.00 .1289 0.003
  7 49.10 .7034
  8 49.50 .7106
 9 49.00 .7140
10 49.70 .7130
 11 49.30 .7053
12 49.30 .7063
 13 49.30 .7053
 14 48.80 .6991
 15 43,40 .6934
                           12.0 -030 -18 39 27 289-07
PTO 69.80
  1 07.40 .1060 -0.061
  2 07.70 .1103 -0.049
  4 06.30 .0903 -0.105
  5 04.70 .0673 -0.159
  6 04.90 .0702 -0.161
  7 45.40 .6934
  8 49.10 .7034
  9 49.30 .7063
 10 49.20 .7045
 11 48,30 .6920
 12 48.30 .6920
 13 47.30 .6777
 14 45.80 .6562
 15 33.90 .4857
```

```
p_x/p_{t,o} \Delta p/q
 TAP
                                       DP Pic Run Test
        \mathbf{p}_{\mathbf{x}}
                              \alpha_{\mathbf{I}}
  PTO 69.80
                              16.0 -030 -13 40 27 280-07
    1 06.50 .0931 -0.097
    2 07.00 .1003 -0.077
    4 02.00 .0287 -0.277
    5 03.20 .0458 -0.229 6 06.50 .0931 -0.037
    7 47.50 .6819
    8 48.50 .6948
    9 48.20 .6905
   10 47.20 .6762
   11 44.90 .6432
   12 45.80 .6562
   13 44.90 .6433
   14 44.20 .6347
   15 21.20 .3037
✓PTO 69.85
                             20•0 -030 -18 41 27 289-07
    1 05.60 .0802 -0.133
    2 06.60 .0945 -0.093
    4 01.90 .0272 -0.281
    5 04.10 .0597 -0.103
    6 06.00 .0859 -0.117
7 42.10 .6027
    8 44.70 .6397
    9 44.00 .6299
   10 42.60 .6099
   11 40.90 .5855
   12 42.90 .6142
   13 42.10 .6027
   14 37.70 .5307
   15 22.30 .3193
  PTO 69.75
                             23.0 -030 -18 42 27 289-07
    1 04.95 .0710 -0.159
    2 06.55 .0939 -0.095
    4 01.75 .0251 -0.287
    5 03.45 .0495 -0.219
    6 05.35 .0767 -0.143
    7 30.55 .5713 3 40.45 .5799
    9 41.55 .5957
   10 40.35 .5785
   11 35.05 .5168
   12 37.65 .5398
   13 36.25 .5197
   14 34.25 .4910
   15 22.75 .3262
```

- .

```
p_x/p_{t,o}^{\Delta p/q}
                          a.
TAP
                                    Ø DP Pic Run Test
      p_x
PTO 59.80
                           00.0 -045 -18 43 27 289-07
  1 08.55 .1225 -0.915
  2 08.25 .1182 -0.027
  4 08.15 .1168 -0.031
  5 08.15 .1160 -0.031 6 03.55 .1225 -0.015
  7 49.75 .7120
  3 49.7" .7128
  9 49.65 .7113
 10 49.75 .7122
 11 49.55 .7113
 12 49.55 .7099
 13 49.45 .7085
 14 49.35 .7070
 15 49.25 .7056
PTO 69.80
                          04.1 -045 -18 44 27 289-07
  1 08.50 .1218 -0.017
  2 03.60 .1232 -0.013
  4 08.30 .1189 -0.025
  5 08.20 .1175 -0.029
  6 09.40 .1347 0.019
  7 50.00 .7163
  3 50.00 .7163
  9 50.10 .7179
 10 50.20 .7192
 11 49,00 .7140
 12 49,80 .7135
 13 49.80 .7135
 14 49.60 .7106
 15 49.60 .7106
                          08-0 -045 -18 /5 27 290-07
PTO '69.80
  1 08.00 .1146 -0.37
  2 08.10 .1160 -0.033
  4 07.50 .1074 -0.057
  5 07.00 .1003 ~0.077
  6 08.40 .1203 -0.021
  7 49.00 .7140
  8 50.00 .7163
  9 50.00 .7163
 19 50 • 10 • 71 79
11 49 • 90 • 71 49
 12 49.60 -7106
 13 49.70 .7120
 14 49.10 .7034
 15 48.40 .6934
```

```
TAP
            p_x/p_{t,o} \triangle p/q
                                      DP Pic Run Test
                           \alpha_{\mathbf{p}}
      \mathbf{p}_{\mathbf{x}}
PTO 69.80
                           12.0 -045 -18 46 27 289-07
   1 07.20 .1032 -0.069
   2 07.30 .1046 -0.065
   4 05.30 .0759 -0.145
   5 04.00 .0702 -0.161
   6 06.20 .0888 -0.109
  7 49.40 .7077
  3 49.80 .7135
  3 49460 -7106
 10 49.30 .7063
 11 49.40 .6904
 12 48.30 .6920
 13 47.00 .6734
 14 43.PO .3275
 15 23:00 :3295
                           16.0 -045 -18 47 27 289-07
PTO 69.75
   1 06.25 .0836 -0.107
   2 06.65 .0953 -0.091
  4 04.45 .0638 -0.179
   5 05.35 .0767 -0.143
   5 06.95 .0996 -0.079
   7 48.35 .6932
  8 48.75 .6989
  9 47.75 .6846
 10 46.85 .6717
 11 43.85 .6287
 12 42.75 .6129
 13 26.55 .5240
 14 34.05 .4882
 15 26.15 .3749
PTO 69.75
                           20.0 -045 -18 48 27 289-07
   1 05.60 .0803 -0.133
   2 06.80 .0975 -0.085
   4 05.10 .0731 -0.153
   5 05.10 .0731 -0.153
   6 06.50 .0932 .007
   7 45 50 6523
   R 46.20 .5624
  9 44.30 .5351
 10 42.20 .5050
 11 37.60 .5301
 12 35.80 .5562
 13 37,40 .5362
 14 33.40 .4789
 15 22.10 .3168
```

```
p_x/p_{t,o} \Delta p/q
TAP
                                    DP Pic Run Test
      P<sub>x</sub>
PTO 69.75
                           23.0 +045 +18 49 27 289+07
  1 05.10 .0731 -0.153
  2 07.50 .1075 -0.057
  4 05.20 .0745 -0.169
  5 04.60 .0659 -1.173
6 05.90 .0846 -0.121
  7 41.40 .5992
  8 43.00 .6165
  9 40.40 .5702
 10 37.40 .5362
 11 32.80 .4703
 12 34,90 .5004
 13 34.50 .4951
 14 27.30 .3914
 15 23.80 .3412
                           23.0 -045 -18 50 27 289-07
PTO 69.75
  1 05.10 .0731 -0.153
  2 07.50 .1075 -0.057
  4 05.20 .0746 -0.149
  5 04.60 .0559 -0.173
  5 05.90 .0846 -0.121
  7 41.80 .5993
  8 43.00 .6165
  9 40.40 .5792
 10 37.40 .5362
 11 32.00 .4703
 12 34,90 .5004
 13 34.60 .4951
 14 27.30 .3916
 15 23.80 .3412
```

OAL 289-8

APPENDIX E TABULATED PRESSURE DATA TABLE III OAL TEST 289-8 M = 2.00

```
p_x/p_{t,o} \Delta p/q
    P<sub>x</sub>
                         \alpha_{\mathbf{z}}
                                 ø
                                      Pic Run Test
TAP
                         00.0 -060.0 1 35 280-08
PTO 69.63
  1 08.43 .1211 -0.019
  2 8.23 .5490 1.177
  4 08.23 .1182 -0.027
  5 08.33 .1196 -0.023
  6 08.73 .1254 -0.007
  7 49.43 .7099
  8 40.53 .7113
 9 49.63 .7128
 10 49.72 .7142
 11 49.83 .7156
 12 49.73 .7142
 13 40.73 .7142
 14 49.53 .7120
 15 49.23 .7070
                        -04.0 -060.0 2 35 289-08
PTO 59.33
  1 08.03 .1159 -0.034
  2 07.73 .1115 -0.046
  4 07.63 .1101 -0.049
  5 07.5% .1090 -0.084
  5 08.23 .1187 -0.025
  7 49,23 .7101
  3 49,43 .7130
 9 49.33 .7115
 10 40.13 .7086
 11 40.13 .7025
 12 49.03 .7072
 13 48.32 .5971
 14 48.53 .7000
 15 48.83 .7042
                          np.n =060.0 3 35 200-08
PTC 59.23
  1 05*13 *1120 -0*050
  2 20,22 ,1120 -1,025
  4 07,83 .1131 -0.041
  5 07.63 .1102 -0.640
  6 08.93 .1203 -0.021
  7 40.43 .7140
  P 49.43 .7140
  9 49.53 .7159
 10 49,63 .7169
 11 40,53 .7154
 12 49.63 .7169
 13 40.72 .7199
 14 49.63 .7169
 15 48 83 .7053
```

```
p_x/p_{t,o} \Delta p/q
TAP
                           a.
                                   ø
                                       Pic Run Test
     \mathbf{p}_{\mathbf{x}}
                           04.0 -060.0 4 35 235-08
PTO 69.53
    <del>_7.52 .5200 _ 1.151</del>
  2 07.63 .1097 -0.051
  4 06.93 .0997 -0.079
  5 06.63 .0954 -0.001
  6 08.03 .1155 -0.034
  7 49.63 .7139
  8 49.83 .7157
  0 49493 .7181
 19 50.03 .7195
 11 49.83 .7167
 12 49.93 .7181
 13 50.13 .7210
 14 50.03 .7195
 15 41.03 .5901
                           04.0 -060.0 5 35 209-06
PTO 69.53
  1 07.53 .1083 -0.054
  2 07.63 .1097 -0.051
  4 06.93 .0997 -0.079
  5 06.63 .0954 -0.091
  6 09.03 .1155 -0.034
  7 49.63 .7133
  8 49.83 .7167
  9 49.93 .7191
 10 50.03 .7195
 11 40.83 .7167
 12 49,03 .7181
 12 50.13 .7210
 14 50,03 .7195
 15 41.03 .5901
                           12.0 -060.0 6 85 289-08
PTC 69.73
  1 06.83 .0979 -1.084
2 05.93 .0994 -1.079
  4 105.83 .0835 -0.124
  5 05.83 .0836 -0.124
  6 08.13 .1166 -h.031
  7 49.53 .7103
  8 49.83 .7146
  9 49.83 .7146
 10 50.03 .7375
 11 49.53 .7102
 12 49.43 .7089
 13 49.73 .7132
 14 49.13 .7046
 15 47.73 .6845
```

```
p_x/p_{t,o} \Delta p/q
TAP
     p_x
                          a.
                                 ø
                                     Pic Run Test
PTO 69.68
                         16.0 -060.0 7 35 285-08
  1 06.78 .0973 -0.035
  2 05.28 .0758 -0.145
  4 04.88 .0700 -0.162
5 04.88 .0700 -0.162
  6 06.28 .0901 -0.105
  7 48.98 .7029
  8 49.38 .7027
  9 49.08 .7044
 10 49.89 .7015
 11 47.78 .6857
 12 47.68 .6843
 13 45,39 .6512
 14 40.18 .5766
 35 40.38 .5795
PTO 69.58
                         20.0 -060.0 9 35 280-08
 1 07.08 .1018 -0.073
  2 05.18 .0744 -0.149
 4 04.98 .0716 -0.157
  5 05.08 .0780 -0.153
  6 05.39 .0772 -0.141
  7 47,88 .5001
  3 48.09 .6910
 7 47.48 .6824
 10 45.58 .6709
 77 47.0F .60AR
 12 25.68 .3691
 13 18,48 .2656
 14 20.79 .2996
 15 37.18 .5242
PTO 69.63
                         27.0 -075.0 0 35 280-08
 1 07.42 .1057 -0.050
  2 05.73 .0823 -0.127
 4 05.03 .0722 -0.155
 5 05.53 .0794 ~0.135
 5 05.03 .0722 -0.155
 7 47.03 65754
 8 47.23 .6783
 0 45.03 .6552
10 40.13 .5763
 11 20.73 .2977
12 16.52 . 2274
13 14.03 .2146
14 17.03 .2446
15 33.73 .4844
```

```
px/pt.o Ap/q a
TAP
                                 ø
     \mathbf{p}_{\mathbf{x}}
                                     Pic Run Test
PTO 69.73
                        -04.0 -075.0 10 35 289-08
  1 08.13 .1166 -0.031
  2 07.83 .1123 -0.043
  4 07.63 .1094 -0.051
  5 07.63 .1094 -0.051
  6 08.33 .1195 -0.023
  7 49.53 .7103
  8 49.73 .7132
  9 49.63 .7117
 10 49.43 .7080
 11 49.43 .7089
 12 49.33 .7074
 13 48.53 .6960
 14 43.82 .7003
 15 49.03 .7031
                        -04.0 -060.0 11 35 299-08
PTO 69.58
  1 09.23 .1181 -0.027
  2 07.83 .1124 -0.043
  4 07.73 .1100 -0.047
  5 07.73 .1300 -0.047
  5 09,43 .12] 3 -0.019
  7 69,63 .7122
  8 49.53 .7151
  3 49.53 .7108
 10 49.33 .7080
 11 49.23 .7065
 12 49.13 .7051
 13 42.03 .6903
 14 48.72 .5003
 15 48.93 .7022
                         00.0 -060.0 12 35 239-08
PTO 69.73
  1 09.33 .1195 -0.023
  2 08.23 .1180 -0.027
  4 08.13 .1166 -0.031
  5 08.23 .1180 -0.027
  6 08.63 .1230 -0.011
  7 49,62 .7117
  8 40.73 .7132
  0 40.63 .7145
 10 40.93 .7160
 11 49.83 .7146
 12 40.73 .7132
 13 49.73 .7132
 14 49.5% .7103
 15 48.93 .7017
```

```
p_x/p_{t,o} \Delta_{p/q}
TAP
                         α
     \mathbf{p}_{\mathbf{x}}
                                 ø
                                      Pic Run Test
                          04.0 -050.0 13 35 289-08
PTO 69.73
  1 09.33 .1195 -0.023
  2 08.33 .1195 -0.023
  4 07.93 .1137 -0.030
  5 07.93 .1122 -0.042
  5 08.73 .1252 -0.007
  7 49.73 .7132
  8 49.93 .7160
  9 50.03 .7175
 10 50.03 .717%
 11 50.03 .7175
 12 50.03 .7175
 13 40.72 .7132
 14 40.82 .7145
 18 49.53 .7102
PTO 69.73
                         08.0 -060.0 14 35 299-08
  1 07.23 .1123 -0.043
  2 08.03 .1152 -0.035
  4 07.43 .1066 -0.059
  5 07.03 .1008 -0.075
  6 09.73 .1352 -0.007
  7 40.92 .7146
  9 40.03 .7150
 9 50.03 .7175
 10 50.03 .7175
 11 40.83 .7146
 12 50.03 .7175
 13 49,93 .7146
 14 49.53 .7103
 15 32.63 .4679
PTO 69.68
                         12.0 -060.0 15 35 280-08
  1 07.08 .1016 -0.073
  2 07.08 .1016 -0.073
  4 05.88 .0844 -0.121
  5 05.08 .0858 -0.117
  6 07.78 .1117 -0.045
  7 49.38 .7037
 8 49.58 .7115
  9 49.53 17115
 10 49.58 .7115
 11 48.58 .6996
 12 49,09 .7020
 13 47.78 .6057
 14 45.18 .6484
 15 17.89 .2565
```

```
p_x/p_{t,o} \Delta p/q
                            ai
                                          Pic Run Test
TAP
     \mathbf{p}_{\mathbf{x}}
                             16.0 -060.0 16 35 280-08
PTO 69.63
1.06.93 .0995 -0.079
   2 06.03 ,0866 -0.115
   4 05.63 .0800 -0.131
   5 05.03 .0722 -0.155
   5 07.03 .1010 -0.075
   7 48.33 .6941
   8 48.73 .6908
   9 48.23 .6927
  10 47.63 .6840
11 45.33 .6510
  12 44.03 .6323
  13 22.53 .3250
  14 11.03 .1574
  15 30.43 .4370
                             20.0 -050.0 17 35 289-08
 PTO 59.68
   1 06.48 .0930 -0.097
   2 05.38 .0772 -0.141
   4 05.18 .0743 -0.150
   5 04.48 .0643 -0.177
6 05.89 .0864 -0.123
   7 45.98 .6508
   8 46.18 .6627
   9 44.39 .6369
  10 41.18 .5910
  11 27.53 .3958
  12 20.98 .3011
  13 12.68 .1820
   14 16.48 .7355
   15 37.98 .5451
                              23.0 -060.0 18 35 289-08
 PTO 69.78
    1 05.08 .4000 -0.078
2 05.88 .0843 -0.122
    4 05.48 .0785 -0.138
    5 04.48 .0642 -0.178
    6 05.08 .0728 -0.154
7 42.78 .6131
    8 42.28 .5059
    9 36.35 .5214
   10 29.58 .4239
   11 18.08 .7591
   12 17.38 .2491
   13 17.39 .2491
   14 13,98 .2003
   15 34.78 .4984
```

```
p_x/p_{t.o} \Delta p/q \alpha_{i}
TAP
     \mathbf{p}_{\mathbf{x}}
                                   Ø
                                       Pic Run Test
PTO 69.58
                           08.0 -060.0 19 35 289-08
  1 07.78 .1118 -0.045
  2 07.88 .1133 -0.041
  4 07.28 .1046 -0.065
  5 06.88 .0989 -0.081
  6 08.58 .1233 -0.013
  7 49.58 .7140
 8 49.78 .7154
  9 49.88 .7160
 10 49.99 .7183
 11 49.68 .7140
 12 49,98 .7183
 13 49,63 .7140
 14 49.38 .7007
 15 31.53 .4539
                           00.0 -090.0 1 36 289-08
PTO 69.91
  1 08.21 .1174 -0.029
  2 08.11 .1160 -0.033
  4 08.21 .1174 -0.029
  5 08.21 .1174 -0.029
6 03.71 .1246 -0.009
  7 49.51 .7082
  8 49.61 .7096
  9 49.71 .7111
 10 49.01 .7125
 11 40.01 .7139
 12 49,91 .7125
 13 40.01 .7130
 14 49.81 .7125
 15 49.63 .7096
                         -04.0 -090.0 2 36 289-08
PTO 60.01
  1,08,11 .3360 -0.033
  2 07.91 .1131 -0.041
  4 07.71 .1103 -0.049
  5 07.71 .1103 -0.0A0
  6 08.31 .1189 -0.025
  7 49.61 .7996
  8 49.71 .7111
 9 69.61 .7096
 10 49.41 .7068
 11 49.41 .7058
 12 49.31 .7053
13 48.71 .6068
 14 49.11 .7025
 15 49.31 .7053
```

```
p_x/p_{t,o} \Delta p/q
TAP
     \mathbf{P}_{\mathbf{X}}
                                  ø
                            \alpha_{L}
                                       Pic Run Test
                          00.0 -090.0 3 36 289-08
PTO 69.86
  1 08.26 .1132 -0.027
  2 08.16 .1168 -0.031
  4 08.16 .1168 -0.031
5 08.16 .1168 -0.031
  6 08.66 .1240 -0.011
  7 49.46 .7080
  8 49.56 .7094
  9 49.66 .7109
 10 49.75 .7123
 11 49.86 .7137
 12 49.75 .7123
 13 49.76 .7123
 14 49.66 .7100
115 49.46 .7080
                          04.0 -090.0 4 36 282-08
PTO 69.86
  1 07.96 .1139 -0.039
  2 08.06 .1154 -0.035
  4 07.96 .1139 -0.039
  5 07.76 .1111 -0.047
  6 08.26 .1182 -0.027
  7 49.85 .7137
  8 49.76 .7123
 9 40.86 .7137
 10 49.86 .7137
 11 49.86 .7137
 12 49.86 .7137
 13 50.06 .7166
 14 50.06 .7166
 15 49.16 .7037
                          02.0 =090.0 5 36 289=08
PTO KO.OS
  1 07.36 .1052 -0.063
  2 07.26 .1038 -0.067
  4 06.84 .0981 -0.083
  5 06436 +0909 -0+103
  6 07.26 .1038 -0.067
  7 40.96 .7141
  8 50.06 .7156
  9 50.06 .7156
 10 50.06 .7156
 11 50.05 .7156
 12 50.16 .7170
 13 50.45 .7213
 14 50.56 .7227
 15 49.66 .7098
```

```
P_x/P_{t,o} \Delta_{p/q}
TAP
     \mathbf{p}_{\mathbf{x}}
                           α,
                                ø
                                      Pic Run Test
                          12.0 -090.0 6 36 289-08
PTO 69.96
  1 07.06 .1009 -0.075
  2 06.66 .0952 -0.091
  4 06.36 .0909 -0.103
  5 06.06 .0066 -0.115
  6 07.56 .1081 ~0.055
  7 40.96 .7161
  8 50.06 .7156
  9 50.06 .7156
 10 50.16 .7170
 11 50.06 .7156
 12 50.46 .7213
 13 49.25 .7141
 14 50.46 .7213
 15 49,96 .7127
PTO 69.86
                          16.0 m090.0 7 36 289m08
  1 07.46 .1068 -0.059
  2 05.06 .0853 -0.119
  4 04.75 .0581 -0.167
  5 05.16 .0739 -0.151
  6 05.56 .0798 -0.135
  7 49466 47109
  8 49.95 .7151
  9 42.86 .7137
 10 50.05 .7166
 11 40.46 .7090
 12 49.16 .7027
 13 47.76 .6537
 14 45.56 .6522
 15 43.86 .6378
                          2(.0 -190.0 8 36 289-08
PTO 69.26
  1 07.66 .1006 -0.051
  2 05.96 .0853 -0.119
  4 04.95 .0710 -0.159
  5 05,06 .0724 -0.155
  5 04.25 .0517 -0.127
  7 49.36 .7137
  9 40.78 .7129
  9 49.36 .7066
 10 49.25 .7051
 11 40.06 .6870
 12 45.26 .6470
 13 37.55 .5391
 14 30.75 .4403
 15 36.16 .5175
```

```
p_x/p_{t,o} \Delta p/q \alpha_{\ell}
TAP
                                    ø
     \mathbf{p}_{\mathbf{x}}
                                       Pic Run Test
                            23.0 -090.0 0 36 280-02
PTO 69.81
   1 08.21 .1176 -0.029
2 06.11 .0875 -0.113
  4 05.51 .0789 -0.137
  5 05.51 .0789 -0.137
  6 04.01 .0574 -0.197
  7 48.91 .6092
  8 49.21 .7049
  9 49.11 .7035
 10 48.11 .6892
11 43.21 .6190
 12 35.21 .5044
 13 25.31 .3626
 14 20.41 .2924
 15 33.61 .4814
PTO 69.81
                            12.0 -090.0 10 36 289-08
  1 07.16 .1026 -0.070
  2 06.66 .0954 -0.091
  4 06.26 .0897 -0.106
  5 06.06 .0868 -0.115
  6 07.56 .1093 -0.054
  7 49.86 .7147
  8 50.06 .7171
  9 40.96 .7157
 10 50.15 .7185
 11 49.96 .7157
 12 50.26 .7200
 13 49.96 .7142
 16 50.36 .7214
 15 49.76 .7123
                            00.0 -090.1 11 36 209-08
PTO 70.15
   1 08.46 .1206 -0.020
   2 09.16 .1163 -0.032
  4 08.26 .1177 -0.128
  5 08.26 .1177 -0.029
6 08.76 .1240 -0.008
7 49.66 .7078
  8 49.56 .7078
  9 49.76 .7092
 10 49 86 .7107
 11 50.06 .7135
 12 49.96 .7121
 13 40.96 .7121
 14 49.86 .7107
 15 49.66 .7078
```

```
p_x/p_{t,o} \Delta_{p/q}
                            \alpha_{\underline{i}}
TAP
     p_{\mathbf{x}}
                                       Pic Run Test
PTO 69.96
                           00.0 -105.0 12 36 289-08
  1 08.46 .1209 -0.019
  2 08.26 .1181 -0.027
  4 08.26 .1181 -0.027
  5 08.26 .1191 -0.027
  6 08.66 .1238 -0.011
  7 49.56 .7084
  8 49.66 .7998
  9 49.55 .7099
 10 49.86 .79.27
 11 49.96 .7141
 12 49.75 .7113
 13 49.85 .7127
 14 49.86 .7127
 15 49.46 .7070
                         -04.0 ~105.0 13 36 289-08
PTO 69.91
  1 08.31 .1189 -0.025
  2 08.01 .1146 -0.037
  4 07.21 .1117 -0.045
  5 07.71 .1103 -0.049
  6 08.51 .1217 -0.017
  7 49.51 .7022
  3 49.61 .7096
9 49.51 .7082
 10 49.31 .7053
 11 49.31 .7053
 12 49.31 .7053
 13 42.41 .6925
 14 49.01 .7010
 15 40.31 .7053
                          04.0 -105.0 14 36 289-08
PTO 69.26
  1 07.96 .1139 -0.039
  2 07.06 .] 130 -0.039
  4 07.76 .1111 -0.047
  5 07.65 .1098 -0.651
  6 03.16 .1168 -0.091
  7 49,76 .7122
  8 49.76 .7123
  9 49.86 .7137
 10 49.05 .7137
 11 69.76 .7123 .
 12 49.86 .7137
 13 49,05 .7151
 14 49.05 .7151
 15 49.46 .7080
```

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```
p_x/p_{t,o} \Delta p/q \alpha_t
TAP
                                     ø
                                         Pic Run Test
      \mathbf{p}_{\mathbf{x}}
                            08.0 -105.0 15 36 280-09
PTO 69.86
  1 07.56 .1082 -0.055
  2 07.26 .1039 -0.067
  4 06.76 .0963 -0.087
  5 06.26 .0396 -0.107
  5 07.06 .1011 -0.075
   7 49.96 .7151
  8 49.96 .7151
  9 49.96 .7151
 10 50.06 .7165
 11 49.95 .7151
 12 49.96 .7151
 13 50.06 .7166
 14 49.56 .7151
  15 Al . 26 . 5020
                            12.0 -105.0 15 36 280-08
PTO 67.96
   1 07.46 .1066 -0.059
   2 06.86 .0981 -0.083
   4 05.46 .0780 -0.139
   5 05.06 .0723 -0.155
   6 05.16 .0708 -0.151
   7 49.96 .7341
   8 50.06 .7156
  9 40.86 .7127
  10 50.06 .7156
  11 49466 47098
  12 49.36 .7055
  13 48.86 .6984
  14 49.05 .7013
  15 45.16 .6234
                             16.0 -105.1 17 36 239-08
PTO 69.96
   1 07.86 .1123 -0.043
2 07.06 .1009 -0.175
   4 05.46 .0750 -0.139
   5 05.16 .0730 -0.151
6 04.76 .0600 -0.157
7 49.46 .7070
   8 49.56 .7024
  9 49.06 .7012
10 49.16 .7027
  11 48.06 .6870
  12 47.56 .6812
  13 44.66 .6304
  14 37.66 .5393
  15 40.56 .5798
```

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```
p_x/p_{t,0} \triangle p/q \alpha_t
                               ø
                                      Pic Run Test
TAP
     \mathbf{p}_{\mathbf{x}}
                          20.0 -105.0 13 36 289-08
PTO 69.91
  1 08.41 .1203 -0.021
  2 07.11 .1017 -0.073
  A 05.91 .0845 -0.121
  5 05.71 .0817 -0.129
  6 04.81 .0688 -0.165
  7 40.61 .0953
  8 48.41 .6925
  0 47.11 .5730
 10 46.81 .6696
 11 41.71 .5966
 12 24.31 .3477
 13 14.31 .2047
 14 17.51 .2505
15 37.21 .5323
PTO 69.86
                          23.0 -105.0 19 36 209-08
  1 08.76 .1254 -0.007
  2 07.46 .1068 -0.059
  4 06.56 .0939 -0.095
  5 06.16 .0382 -0.111
  6 04.96 .0710 -0.150
  7 47.65 .5022
  3 47.26 .6765
  9 44.56 .6203
 10 30.06 .5720
 11 21.26 .3743
 12 15.06 .2156
 13 12.56 .1708
 14 14.86 . 2127
 15 32.35 .4775
                          12.0 -105.0 20 36 235-09
PTO 70.16
  1 07.76 .1106 -0.049
  2 06.96 .0992 -0.090
  4 05.35 .0764 -0.144
  5 06.16 .0725 -0.152
  6 04.36 .3593 -0.163
  7 40.75 .7002
  8 49,96 .7121
  9 49.46 .7050
 10 49.56 .70.78
 11 48.26 .6064
 12 48.56 .5921
 13 47.06 .6709
 14 66.05 .6220
 15 43.36 .5180
```

ı

```
px/pt.o Dp/q a
TAP
    P_{\mathbf{x}}
                                  Ø Pic Run Test
PTO 69.96
                          12.0 -105.0 21 36 289-08
  1 07.46 .1066 -0.053
  2 05.86 .0981 -0.083
 4 05.46 .0780 -0.139
 5 04.96 .0709 -0.159
  6 05.16 .0738 -0.151
  7 49.96 .7141
  8 50.06 .7156
 0 49.86 .7127
 10 50.06 .7156
 11 40.66 .7098
 12 49.35 .7055
 13 48.86 .6934
 14 49.06 .7013
15 48.16 .6984
PTO 70.16
                         00.0 -105.0 22 36 289-09
  1 08.36 .1192 -0.124
  2 03.26 .1177 -0.028
 4 08.26 .1177 -0.028
 5 08.26 .1177 -0.023
 6 08.66 .1234 -0.012
 7 49.66 .7079
.8 49.66 .7072
9 49.76 .7092
10 49.96 .7121
 11 49.86 .7107
 12 49.96 .7107
13 40,06 ,7121
 14 49.96 .7121
 15 49.46 .7050
PTC 69.96
                         CO.0 -120.0 23 36 280-08
  1 08.56 .1224 -0.015
  2 09.26 .1181 -0.027
  4 08.25 .1181 -0.027
  5 08.26 .1191 -0.027
  6 08.65 .1230 -0.011
7 49.45 .7070
  3 49.56 .7084
 0 49.76 .7113
 10 42.96 .7141
11 49.95 .7127
 12 49.76 .7113
 13 45.85 .7127
 14 49.66 .7098
 15 49.26 .7041
```

```
Px/Pt,0 Dp/q at
TAP
                                 ø
     p_{\mathbf{x}}
                                     Pic Run Test
PTO 69.98
                        -04.0 -120.0 24 35 289-08
  1 08,46 .1209 -0.019
   2 07.96 .1130 -0.039
  4 07.96 .1132 -0.039
   5 07.86 .1123 -3.043
  6 08.86 .1265 -0.003
  7 49.65 .7098
  8 49.75 .7113
  9 49,56 .7084
 10 49.46 .7070
 11 47.46 .7070
 12 49.15 .7027
 13 48.16 .6934
 14 49.06 .7013
 15 49.26 .7041
PTO 69.96
                         04.6 -120.0 25 36 239-08
  1 08.16 .1166 -0.131
  2 07.96 .1138 -0.039
  4 07.96 .1138 -0.039
  5 07.76 .1109 -0.047
  6 08.26 .1181 -0.027
  7 49.76 .7113
  8 45.86 .7127
  9 49.86 .7127
 10 49.96 .7141
 11 50.00 .7156
 12 50.06 .7155
 13 49.95 .7127
 14 49.86 .7127
 15 49.66 .7098
PTO 69.81
                         08.0 -120.0 25 36 289-08
  1 07.71 .1104 -0.049
  2 07.41 .1061 -0.061
  4 06.91 .0990 -0.000
  5 06.41 .0918 -0.101
  ล 07.21 .1033 ⊷0.162
  7 40.91 .7135
  P 49,61 .7140
  9 49.81 .7135
 10 49.01 .7149
 11 45.81 .7135
 12 49.31 .7135
 12 49.71 .7121
 14 49.21 .7063
 15 23.01 .4857
```

```
TAP
     \mathbf{p}_{\mathbf{x}}
           p_x/p_{t,0} \Delta p/q \alpha_z
                                    ø
                                        Pic Run Test
PTO 70.11
                            12.0 ~120.0 27 25 250-02
   1 97.71 .1100 -0.050
   2 07.31 .1043 -0.056
   4 06.31 .0900 -7.106
   5 05.71 .0916 -0.130
   6 06.41 .0914 -n.10?
   7 49.81 .7105
   8 49.81 .7105
  0 40,41 .7047
 10 49.61 .7076
 11 49.01 .6990
 12 48.81 .6962
 13 47.51 .6776
 14 44.71 .6377
 15 17.71 .2526
PTO 70.16
                            16.0 -120.0 28 36 289-08
  1 08.11 .1155 -0.024
   2 07.61 .1085 -0.054
  4 06.41 .0914 -0.102
  5 06.11 .0871 -0.114
  6 05.51 .0942 -0.094
  7 49.21 .7014
  8 49.01 .6985
  9 48.01 .6942
 10 45.11 .6857
 11 45.21 .6601
 12 44.21 .6301
 13 27.61 .3200
 14 00 81 130°
 15 27.61 .3035
PTO 70.15
1.06.31 .1256 -0.006
                           20.0 -120.0 20 36 200-00
  4 06.91 .0995 -0.082
5 05.81 .3971 -3.086
  6 07.11 .1012 -0.074
7 47.01 .6700
  8 46.31 .5501
 9 43.41 .61P7
10 41.31 .5998
 11 20.01 ./406
 12 22.11 .3151
 13 17-47 .2481
 14 18.01 .2567
 15 32.21 .5446
```

```
p_x/p_{t,o} \triangle p/q \alpha_z
TAP
     \mathbf{p}_{\mathbf{x}}
                                  ø
                                       Pic Run Test
PTO 70.01
                          22.0 -120.0 30 36 280-08:
  1 09.46 .1351 0.020
  2 08.86 .1266 ~0.003
  4 07.56 .1080 -0.055
  5 07.46 .1066 -0.059
  5 07.56 .1080 -0.055
  7 43.95 .6279
  3 41.65 .5951
  9 35.05 .5009
 10 30.05 .4422
 11 22.76 .3251
 12 18.66 .2665
 13 21.66 .3096
 14 14.76 .2100
 15 33.35 .4836
PTO 70.16
                          12.0 -120.0 31 36 289-08
  1 07.71 .1099 -0.050
  2 07.31 .1042 -0.066
  4 06.31 .0899 -0.106
  5 05.71 .0314 -0.130
  6 06.41 .0014 -0.102
  7 49.91 .711/
  9 49.91 .711A
9 49.61 .7071
 10 49.71 .7085
 11 45.01 .6095
 12 48 31 6057
 13 47.51 .6772
 14 44.61 .6353
 15 17.31 .2467
                          00.0 -120.0 32 36 200-08
PTO 69.96
  1 08.46 .1209 -0.019
  2 05.15 .1166 -0.031
  4 08.25 .1181 -0.027
  5 00.26 .1121 -0.027
  6 08.66 .1238 -0.011
  7 49.46 .7070
  S 40.66 .7099
 9 49.36 .7127
 10.49.96 .7141
 11 49.35 .7127
 12 49.26 .7127
 13 69.PF .7127
 16 40.75 .7113
 15 49.25 .7041
```

```
p_x/p_{t,o} \Delta p/q
TAP
                         a<sub>z</sub>
                                      Pic Run Test
     \mathbf{p}_{\mathbf{x}}
PTO 69.91
                          00.0 -135.0 33 26 289-03
  1 08.51 .1217 -0.017
  2 08.21 .1174 -0.029
  4 08.21 .1174 -0.029
  5 08.21 .1174 -0.029
  6 08.71 .1245 -0.009
  7 49.51 .7082
  8 49.71 .7111
  9 49.81 .7125
 10 49.81 .7125
 11 49.71 .7113
 12 49.61 .7096
 13 49.41 .7068
 14 49.31 .7053
 15 49.21 .7039
                          04.0 -135.0 34 36 289-03
PTO 69.91
  1 08.31 .1199 -0.025
  2 08.11 .1160 -0.033
  4 08.01 .1146 -0.037
  5 07.91 .1131 -0.041
  6 08.41 .1203 -0.021
  7 49.61 .7096
  8 49.81 .7125
 9 49.81 .7125
 10 50.01 .7153
 11 49.91 .7139
 12 49.81 .7125
 13 49.71 .7111
 14 49.61 .7095
 15 49.61 .7096
PTO 69.95
                          ne•n =135•n 35 36 289≈08
  1 07.86 .1123 -0.043
  2 07.65 .1095 -0.051
  41.07.36 .1052 -0.063
  5 05.95 .0905 -0.079
  5 07.76 .1100 -0.047
  7 49.56 .7084
  8 49.65 .7008
  9 49.55 .7094
 10 49.86 .7127
 11 49.76 .7113
 12 49.36 .7055
 13 49.55 .7084
 14 48.86 .6984
 15 47.15 .6741
```

```
p_x/p_{t,o} \Delta p/q \alpha_z
TAP
     \mathbf{p}_{\mathbf{x}}
                                       Pic Run Test
PTO 69.96
                          12.0 -135.0 36 36 289-08
  1 07.86 .1123 -0.043
  2 07.56 .1031 -0.055
  4 07.06 .1009 -0.075
  5 06.65 .0952 -0.091
  6 07.66 .1095 -0.051
  7 49.48 .7070
  8 49.36 .7055
  9 48.86 .6984
 10 48.96 .6092
 11 48.16 .6884
 12 47.96 .6855
 13 46.46 .5641
 14 43.06 .6155
15 21.75 .3110
PTO 69.96
                          16.0 -135.0 37 36 200-08
  1 08.36 .1195 -0.023
2 07.86 .1123 -0.043
  4 07.36 .1052 -0.063
  5 07.16 .1023 -0.071
  6 08.36 .1195 -0.023
  7 48.76 .6970
  9 48.35 .6912
  9 45.65 .5570
 10 46.76 .6684
 11 44.45 .5355
 12 42.56 .6083
 13 37.35 .5340
 14 34.06 .4268
 15 25.56 .2654
PTO 69.16
                          20.0 -135.0 38 26 289-08
  1 09.06 .1795 0.105
  2 08.46 .1209 ⊷1.019
  4 08.05 .1152 -0.025
  5 08.06 .1152 -0.035
  5 09.26 .1324 0.013
  7 45.76 .6504
  8 45.86 .6555
 9 42.76 .5112
 10 42.06 .6012
 11 30.06 .5503
 12 38.76 .5540
 13 38.15 .5455
 14 32.96 .4711
 15 21.45 .3067
```

- -

```
p_x/p_{t,o} \Delta_{p/q}
TAP
                            a.
                                       Pic Run Test
     \mathbf{p}_{\mathbf{x}}
PTO 69.96
                          23.0 -135.0 39 36 289-08
  1 00.95 .1424 0.041
  2 09.06 .1295 0.005
  4 08.86 .1266 -0.003
  5 08.86 .1266 -0.003
  6 10.16 .1452 0.049
  7 43.96 .5234
  8 42455 46023
  9 37.05 .5297
 10 37.76 .5397
 11 34.96 .4003
 12 34.76 .4960
 12 35.16 .5026
 14 26.76 .3525
 15 23.56 .3363
PTO 70.11
                          12.0 -135.0 40 36 289-08
  1 08.01 .1142 -0.030
  2 07.61 .1085 -0.054
  4 07.11 .1014 -0.074
  5 06.71 .0957 -0.090
6 07.71 .1100 -0.050
  7 49.61 .7076
  8 49.51 .7062
  9 48.01 .5976
 10 49.01 .6930
 11 48.21 .6875
 12 42.01 .6042
 13 46.41 .6620
 14 42.01 .6120
 15 21.51 .3069
PTO 70.06
1 05.46 .1268 ↔0.020
                          00.0 -105.0 41 36 284-08
  2 08.25 .1179 -0.028
  4 08.25 .1179 -0.028
  5 08.26 .1179 -0.029
  6 00.66 .1235 -0.012
  7 49.66 .7088
  8 49.76 .7102
 9 40.86 .7117
 11 49.76 .7102
 12 49456 47074
 13 40.46 .7080
 14 49.36 .7045
 15 40.36 .7045
```

OAL 289-10

APPENDIX E TABULATED PRESSURE DATA TABLE IV OAL TEST 289-10 M = 2.00

TAP	p _x	p _t /p _{t,o} Δ p/q	a.	ø	Pic Run Test
PTO	72.33		20.40	000.0	1 29 289+10
		•1269 mn•102			14 7. 2. 3. 4. 2. 3. 3. 3. 1.
2	08,68	•1200 ←0•^22			
		•1228 -0•014			
		•1228 - 0•014			
		•1255 - 0•006			
	50.48				
	49.88 50.38				
	50.68				
11					
	50.78				
	50.79				
	50,05	•			
1.5	51.08	.7062			
PTO	72.13		$C \bullet C$	$0.000 \cdot 0$	2 29 289→10
3		•1359 - 0•005			
2	08•68	•1203 - 0•021			
۷,	09_88	.1231 -0.013			
		.1231 -0.013			
		.1250 -0.005			
	50.28				
8.	49.68	•6288			
ċ	50.03	. 6942			
-	50.43	•			
	50.68				
	50,62				
	50.68				
	50.78 50.28				
1.37	1117 4 M 4	• 7 C 37k			
PTO	72.13		o'	145.0	3 29 289+10
		.1250 - 0.005	-		
2	08.68	.1202 - 0.021			
Α.	63,68	*1531 -0 *013			
		*1551 -0*013 *1503 -0*051			
7		705/			
	-	7026			
ó	50,63	7026			
3.0	50,60	.712c			
1.1	20° 80	• 7954			
1. ?	50.28	• 70F4			
13	50,00	.7060			
14	50.00	- 7068			
15	ֆ Ո •08	• 7063			

TABLE IV GAL TEST 289-10 M = 2.00

```
p_x/p_{t,o} \Delta p/q
                          2
                                      Pic Run Test
TAP
     p_x
PTO 72.38
                         00.0 -045.0 4 29 289-10
  1 09.08 .1254 -0.007
  2 08.69 .1199 -0.022
  4 08.88 .1227 -0.014
  5 (2.48 .1190 -0.022
  6 08.98 .1241 -0.010
  7 51.38 .7000
  9 51.48 .7110
 9 51,20 .7085 -
 10 51.38 .7000
 11 51,48 .7112
 12 51.38 .7099
 13 21.38 .2000
 16 51,29 .7085
 15 50.08 .7043
PTO 72.23
                         00.0 -090.0 5 29 299-10
 1 08,68 .1200 -0.021
  2 00.28 .1146 -0.037
 4 09,68 .1202 -1.021

    ∪8,68 *1505 *0*351

 6 08.89 .1229 -0.014
 7 51.28 .7100
 9 51.38 .7112
 9 51.28 .7100
 30 51.48 .7127
 11 51.68 .7155
 12 51.68 .7127
 13 51.38 .7113
14 51.38 .7113
15 51.33 .7113
                         04.0 -035.0 6 29 280-10
PTO 72.28
 1 05.08 .1056 -0.006
 2 08.68 .1201 -0.021
 4 08,88 .1229 -0.014
 5 09.58 .1107 -0.005
 6 00,08 .1381 0,000
 7 51.18 .70(1
 8 51.48 .7122
 0 51.48 .7122
 10 51.28 .7395
 11 51.38 .7109
12 51.28 .7005
13 51.28 .7005
14 51.18 .7021
 15 51.03 .7067
```

TABLE IV OAL TEST 289-10 M - 2.00

.....

. . .

```
px/pt.o Dp/q a
                                       ø
TAP
                                           Pic Run Test
     p_{\mathbf{x}}
 PTO 72.18
                             04.0 -040.0 7 29 289-10
   1 08.98 .1244 -0.009
   2 08.68 .1203 -0.021
   4 08.88 .1230 -0.013
   5 08.48 .1175 -0.029
   6 09.88 .1369 0.025
   7 51.28 .7104
   8 51.48 .7132
   9 51,58 ,7146
  10 51.43 .7132
11 53.38 .7119
  12 51.38 .7118
  13 51.28 .7104
14 51.18 .7091
  15 51.18 .7001
PTC 72.18
                             04.0 -050.0 8 29 289-10
   1 08.88 .1230 -0.013
   2 08.68 .1209 -0.001
   4 08.78 .1216 -0.017
   5 08.38 .1151 -0.032
   6 09.38 .1200 0.006
  7 51.48 .7132
  8 51.38 .7118
 9 51.58 .7146
10 51.68 .7160
  11 51.78 .7174
  12 51.48 .7132
 13 51.38 .7713
 14 51,38 .7119
 15 53,18 ,7091
PTO 71.98
1 08.88 .1334 -0.012
                             04.6 -055.0 9 29 289-10
  2 08.58 .1192 -9.024
   4 08.68 .1206 ~0.020
  5 09.28 .1150 -0.036
6 09.18 .1275 -0.001
7 51.28 .7124
 8 51.18 .7110
9 51.49 .7150
10 51.49 .7150
 11 51.58 .7165
 12 51.58 .7166
 13 51.28 .7124
 14 51.38 .7138
 15 51.08 .7096
```

TABLE IV OAL TEST 239-10 M = 2.00

```
p_{x}/p_{t,o} \triangle p/q
                                   ø
?'AP
     p_{\mathbf{x}}
                          a.
                                       Pic Run Test
                          04.0 -060.0 10 29 289-10
PTO 71.48
  1 08.68 .1214 -0.018
  2 08.38 .1172 -0.030
  4 08.48 41186 -0.026
  5 08.18 .1144 -0.037
  6 08.93 .1242 -0.010
  7 51.08 .7146
  8 51,08 .7146
  9 51.03 .7146
 10 51,18 .7160
 11 51.28 .7174
 12 51.38 .7129
 13 51.08 .7146
 14 51,18 .7160
 15 50.08 .7118
                          04,0 -065,0 11 29 289-10
PTO 71.38
  1 08.73 .1228 -0.015
  2 08.33 .1167 -0.031
  4 08,43 .1181 -0.027
  5 08.13 .1130 -0.030
  6 08.73 .1223 -0.015
  7 51.03 .7149
  8 51.03 .7145
  9 51.13 .7167
 10 51.13 .7168
 11 51.23 .7177
 12 51, 22 ,7191
 13 51.23 .7177
 14 51.13 .7163
 15 50,83 .7121
                         -04.6 -070.0 l2 29 280<del>-</del>10
PTO 71,53
 1 02.58 .1100 -0.022
  2 08,28 ,1159 -0,033
  4 00,28 .1172 -0.030
  5 07,08 .1116 -0,045
  6 08.68 *4318 -0.018
  7 51.00 .7141
  9 51.69 .7161
  9 53 4 10 . 73 50
 10 51.18 .7155
 11 51.18 .7155
 12 51.08 .7160
 13 51,28 .7159
 14 51.28 .7160
 15 50.88 .7113
```

TABLE IV OAL TEST 289-10 M = 2.00

```
p_{x}/p_{t,o} \stackrel{\Delta}{=} p/q
TAP
                                    ø
                                       Pic Run Test
     \mathbf{p}_{\mathbf{x}}
PTO 71.43
                           04.0 -150.0 13 29 289-10
  1 08.58 .1201 -0.001
  2 08.18 .1145 -0.037
  4 00.49 .1187 -0.025
  5 08.18 .1145 -0.037
  6 08.68 .1215 -0.038
  7 50.68 .7095
  8 50.58 .7091
  9 50,48 .7057
 10 50.48 .7067
 11 50,58 47091
 12 50.48 .7067
 13 50,48 .7067
 14 50,39 ,7053
 15 50.28 .7039
                          04.0 -165.0 14 29 290-10
PTO 71,23
  1 00.58 .1205 -0.000
  2 08.28 .1162 -0.032
  4 በ8.58 .1209 <del>-</del>0.020
  5 08.33 .1176 -0.0000
  5 09.78 .1239 -0,072
  7 40.85 .7002
  8 50.09 .7031
 9 50.08 .7031
 10 40,98 .7017
 11 45,09 .7017
 12 49,58 .7003
 13 40678 .50PO
 14 49.78 .0000
 15 40,68 .6975
PTO 70.93
                          04.0 mise.0 is 20 200min
 1 00.48 .1196 -0.123
  2 00.18 .1152 -0.036
 6 08.48 .1105 -0.003
5 08.48 .1106 -0.002
  6 08.88 .1252 -0.107
 7 49.38 .5652
 2 40.48 .8976
 0 49,48 5075
 11 40458 45900
 12 49,58 ,6990
 13 40,52 .5000
14 49,58 .6090
 15 49.38 .6062
```

TABLE IV OAL TEST 289-10 M = 2.00

```
p_{x}/p_{t,0} \Delta p/q \alpha_{t}
"PAP
                                       Pic Run Test
     \mathbf{p}_{\mathbf{x}}
                         08.0 -180.0 16 29 289-10
PTO 71.33
  1 08.48 .1189 -0.025
  2 08.08 .1133 -0.040
 4 08.48 .1189 -0.025
  5 08.58 .1208 -0.021
  8 00.18 .1207 C.003
  7 40,29 .6900
  8 69,08 6881
 9 48,98 .6957
 10 90 00 92601
 11 40,09 ,6291
 12 48,98 .6867
 13 48.78 .6839
 14 48.68 .6925
 15 47.99 .6712
                         08.0 -165.0 17 29 289-10
PTO 71.38
  J 08.48 .1188 -0.025
  2 09.08 .1132 -0.041
  4 08,58 .1202 -0.021
  5 09.28 .1160 -0.023
  5 09,08 .1272 -0,002
  7 49.68 -6960
  8 49.68 .6960
  9 49,63 ,6960
 10 49.88 .5988
 11 40.78 .5974
 15 60.70 .6074
 13 49.68 .6960
 14 49.40 .5032
 15 45.75 .6834
                         -00•0 -150•0 18 29 209-10
PTO 71,33
 1 05.28 .1161 -0.023
  2 07.88 .1105 -0.048
  4 09.28 .1151 -0.033
  5 07.6P .1077 -0.056
  6 08,48 .1200 -0.021
  7 50479 .7069
  3 50.28 .7063
  0 50,39 ,7062
 10 50, 58 . 7001
 11 50,59 .7091
 12 50.48 .7077
 13 50.20 .7049
 14 40.83 .6933
 15 49,28 .6999
```

1

TABLE IV OAL MET 289-10 M = 2'.00

```
p_x/p_{t,o} \Delta p/q
TAP
                             \alpha_{\mathbf{k}}
                                          ¢
                                               Pic Run Test
      \mathbf{p}_{\mathbf{x}}
PTO 71.38
                               06.0 -070.0 19 29 289-10
  1 08.08 .1132 -0.041
  2 07.68 .1076 -0.056
  4 07.58 .1062 -0.060
  5 07.18 .1006 -0.076
  6 08.38 .1174 -1.029
  7 50.93 .7142
  8 51.08 .7156
  9 51.18 .7170
 10 51.28 .7184
 11 53.08 .7156
 12 51408 •7156
 13 51.28 .7184
14 51.18 .7170
 15 41.78 .5852
                               00.0 -065.0 20 29 289-10
PTO 71.23
  1 08.18 .1148 -0.036
  2 07,88 .3106 -0.048
  4 07.68 .1078 -0.056
  5 07.28 .1022 -0.772
  5 08,58 .1205 -0.020
  7 50.78 .7120
  9 50,08 .7157
  9 50,98 .7157
 10 51.0P .7171
 11 50 688 47163
12 50 68 47157
 13 51,08 .7171
 14 50.78 .7129
15 38.98 .5472
PTO 71.13
1 02.18 .1150 ~0.036
                               08.0 -060.0 21 29 289-10
  2 07.92 .1172 -7.044
  4 07.68 .1000 ~1.055
5 07.38 .1000 ~0.067
6 00.78 .1236 ~0.012
7 50.68 .7125
 8 50.08 .7153
9 50.03 .7157
10 50.03 .7167
 11 50,78 .7139
 12 50.88 .7152
 13 50.29 .7153
 14 50.68 .7125
 15 38.08 .5354
```

APPENDIX E (CORF'D)

TABLE IV OAL TEST 289-10 M * 2.00

```
p_x/p_{t,o} \Delta_{p/q} \alpha_{e}
TAP
     p_{\mathbf{x}}
                                       Pic Run Test
PTO 70.88
                          08.0 -055.0 22 29 289-10
 1 03.28 .1168 -0.031
  2 07,59 .1326 -0.042
  4 07.68 .1094 -0.054
  5 07.38 .1041 -0.064
  6 08.79 .1233 -0.011
  7 50.58 .7125
  8 50.68 .7150
  0 50,68 ,7150
 10 50.79 .7164
 11 50,58 .7336
 12 50,68 .7150
 13 50.68 .7150
 14 50.28 .7004
 15 40,68 .5739
210 71.18
                         -08.0 -050.0 23 29 289-10
 1 08.38 .1177 -0.028
  2 08.09 .1135 -0.040
  4 07,88 .1107 -0,068
 5 07,28 .1037 -0.067
  6 00.69 .1210 -0.016
 7 50.78 .7134
 8 50.89 .7169
 0 50,98 .71/9
 10 50,50 .7162
 11 50,68 .7120
 12 50.38 .7070
 13 50.78 .7134
14 50,28 .7056
15 65,88 .6646
                         00.0 -060.0 26 20 200-10
PTO 70.03
 j 00,38 ,1191 -0,027
  2 08.18 .1152 -0.035
 4 07.98 .1125 -0.043
 5 07,19 .1012 -1.074
 A 00.48 .1105 -".028
 7 50.18 .7075
 8 50.38 .7108
 9 50,52 .7131
 10 50,59 ,7121
 11 50.58 .7191
12 50.38 .7103
 13 50.18 .7075
 14 49,78 .7110
 15 49.13 .5034
```

TABLE IV OAD THOT 289-10 M = 2-00

TAP	$p_{\mathbf{x}}$	$p_x/p_{t,o} \Delta p/q$	æ	ø	Pic Run Test
1		•1189 -0•025 •1161 -0•033	08+0	-035 .0	25 29 289-10
5 7 8 9 10 11 12 13	07.28	.7097 .7119 .7139 .7105 .7077 .7049			
1,		.1005 -0.051 .1052 -0.063	12.0	₩035 , 0	26 29 289-10
5 6 7 8 9 10 11 12 13	04.88	.7032 .7022 .7017 .6877 .6219 .6764			
1		.1040 -0.055 .1024 -0.071	12.0	- 040.0	27 29 289-10
5 6	05.28 49.79 50.28 50.10 49.88	.7003 .7074 .7060 .7017 .6877 .6905 .5708			

TABLE IV OAL TEST 289-10 M = 2.00

```
p_x/p_{t,o} \Delta p/q
TAP
                                  ø
                                     Pic Run Test
     p_{\mathbf{x}}
PTO 71.08
                         12.4 -050.0 28 29 289-10
  1 07.48 .1052 -0.063
  2 07.08 .0996 ~0.079
  4 06.08 .0855 -0.118
  5 05.48 .0771 -0.142
  6 06.88 .0968 -0.027
  7 50,28 .7074
  8 50.58 .7116
  9 50,48 ,7102
 10 50.18 .7060
 11 40,28 .6933
 12 40.25 .6947
 13 47.78 .6727
 14 44.08 .6201
 15 19.88 .2797
PTO 71.13
                         12.0 -055.0 29 29 289-10
 1 07.48 .1052 -0.063
  2 07.08 .0995 -0.079
 4 05.13 .0869 -0.114
 5 06,13 .0350 -0.114
  6 07.09 .0005 -0.079
 7 50.38 .7083
 8 50.68 .7125
 9 50.42 .7097
 10 50.33 .7023
 11 40.58 .6070
 12 49.68 .5984
 13 48,48 .5016
 14 45,28 ,5266
 15 19.78 .2660
PTO 71.08
                         12.0 -060.0 30 25 289-10
  1 07.38 .1039 -0.067
 2 07.08 .0296 -0.679
 A 06.28 .0384 -0.110
 5 06.58 .0326 -0.000
 6 00.18 .1151 -0.035
7 50.28 .7074
 8 50.59 .7116
 9 50.58 .7116
 10 50,48 .7102
 11 49.78 .7003
 10 40,08 47030
 13 49.18 .6919
14 47.08 .6824
 15 19.18 .2698
```

TABLE IV OM 1887 289-10 M = 2.00

```
px/pt,o Dp/q a
TAP
                                   ø
                                       Pic Run Test
     \mathbf{p}_{\mathbf{x}}
PTO 70.98
                          12.0 -065.0 31 29 289-10
  1 07.28 .1026 -0.070
  2 07.18 .1012 -0.074
  4 06.28 .0S85 -0.110
  5 06.68 .0941 -0.094
  6 08.78 .1237 -0.011
  7 50.18 .7070
  8 50.58 .7126
  9 50.68 .7140
 10 50.58 .7126
 11 49,93 .7041
 12 50.28 .7084
 13 49.78 .7012
 14 4P#68 #6P58
 15 28,28 .3984
                          12.0 -070.0 32 29 289-10
PTO 70.93
  1 07.05 .0998 -0.078
  2 07.18 .1012 -0.074
  4 06.28 .0885 -0.110
  5 07.08 .0998 -0.078
  6 08.48 .1196 -0.023
  7 50.38 .7109
  8 50.63 .7145
  9 50.68 .7145
 10 50.68 .7145
 11 50.28 .7080
 12 50.00 .7060
 13 49.88 .7032
 14 49.68 .7004
 15 47.08 .653E
                          12.0 -150.0 33 29 289-10
PTO 71.03
  1 08.28 .1166 -0.731
  2 07.78 .1095 -1.051
  4 05.28 .1166 -0.031
  5 07.00 .1100 -0.047
6 09.08 .1278 0.000
  7 49.88 .7022
  8 49.00 .7036
  9 49,48 .6366
 10 49.78 .7008
 11 49.28 .6938
 12 48.98 .6896
 13 48.08 .6769
 14 46.65 .6572
 15 36.23 .5108
```

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APPENDIX E (COMP'D)

TABLE IV OAL TEST 289-10 N = 2.00

```
p_x/p_{t,o} \triangle p/q
TAP
                                  ø
     \mathbf{p}_{\mathbf{x}}
                        CK
                                       Pic Run Test
PTO 70.83
                          12.0 -165.0 34 29 289-10
  1 08458 41213 -04019
  2 08.08 .1141 -0.038
  4 08.38 .1254 -0.007
  5 08.88 .1254 -0.007
  6 09.88 .1395 0.033
  7 48,68 .6872
  8 47.08 .6774
  9 47,29 .6675
 10 49,08 .6929
 11 49,00 ,6015
 12 48.78 .6237
 13 48.18 .6872
 14 47.28 .6675
 15 46.28 .6534
PTO 70.93
                         12.0 -180.0 35 29 289-10
  1 08.78 .1238 -0.017
  2 08.18 .1153 -0.035
  4 09.08 .1280 0.001
  5 00.39 .1222
                 0.4013
  6 10,18 .1435 0.044
  7 49,09 ,6919
  8 48.38 .6021
  9 67,58 ,5722
 10 47.48 .6694
 11 46.58 .6567
 12 45.79 .6454
 13 44.28 .6243
 14 47.88 .6750
 15 46.38 .6530
                         16.0 -180.0 36 29 289-10
PTO 70.58
 1 09.13 .1205 0.005
  2 08.58 .1210 -0.019
  4 09.88 .1304
                 0.033
  5 10.69 .1507 0.064
  6 12:08 -1704
                 ( .119
  7 49.38 .6957
  8 48.18 .6797
 9 47.08 .6642
 10 47.19 .6556
 11 45.09 .6607
 12 46.98 .6346
 13 42,88 .6050
 14 40.48 .5711
 15 41.88 .5000
```

TABLE IV OAL TEST 239-10 H = 2.00

```
p_x/p_{t,o} \triangle p/q \quad \alpha_c
                                       Pic Run Test
TAP
     p_{\mathbf{x}}
PTO 70.83
                          16.0 -165.0 37 29 289-10
  1 08.88 .1254 -0.007
  2 08.38 .1183 -0.027
  4 09.58 .1367 0.025
  5 09.88 .1395 0.033
  6 11,48 -1621 0.096
  7 47.88 46760
  8 46.78 .6605
 9 45•28 •6393
 10 45.18 .6370
 11 47.00 .6647
 12 46.48 .6562
 13 44,38 .6336
 14 42.88 .6054
 15 41.28 .5828
PTO 70.83
                          16a0 -150a0 38 29 289+10
  1 08.48 .1197 -0.023
  2 08.03 .1141 -0.038
  4 08,88 .1254 -0.007
  5 08.88 .1254 -0.07
  6 10.18 .1437 0.044
  7 48.78 .6837
 8 49.18 .6943
 9 47.88 .6760
 10 48,08 .5788
 11 46.38 .5548
 12 46.38 .6548
 13 45.88 .6477
 14 44.58 .6302
 15 22.68 .3202
PTO 70.33
                          16.0 -070.0 39 29 289-10
  1 05.88 .0830 -0.125
  2 05.98 .0844 -0.121
  4 05.28 .0745 -0.149
5 07.08 .1000 -0.078
  6 05,55 .0929 -0.197
  7 49.42 .5986
 9 49,08 ,7056
 10 49,58 .7000
 11 48.18 .6802
 12 47,98 .6774
 13 44.68 .6308
 14 28.88 .4077
 15 39.08 .5517
```

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TABLE IV OAL TEST 289-10 M = 2.00

```
p_x/p_{t,o} \Delta p/q \alpha_t
                                   ø
                                        Pic Run Test
TAP
     \mathbf{p}_{\mathbf{x}}
PTO 70.88
                           16.0 -065.0 40 29 289-10
  1 05.78 .0815 -0.129
  2 06.28 .0886 -0.110
  4 05.68 .0801 -0.133
  5 06.08 .0858 -0.117
  6 06.78 .0957 -0.090
  7 49.48 .6981
  8 49,78 .7022
  9 49.48 .6981
 10 49.28 .6952
 11 47.58 .6713
 12 45.88 .5614
 13 39.68 .5598
14 18.88 .2664
 15 32.38 .4568
PTO 71.08
                          16.0 -060.0 41 29 289-10
  1 06.78 .0954 -0.091
  2 06.18 .0869 -1.114
  4 05,98 .0841 -0.122
  5 05,98 .0841 -0.122
  6 07.18 .1010 -0.075
  7 49.38 .5047
  8 49.78 .7003
  9 49.38 .6947
 10 48.88 .6877
 11 46,08 +6595
 12 45.62 .6427
 13 29.58 .4176
 14 12.88 *1312
 15 25.08 .3528
                          16.0 -055.0 42 29 289-10
PTO 71.43
 1 06.88 .096% -0.00%
  2 06.13 .0865 -0.115
  4 05.38 .0823 -0.127
  5 05.98 .0837 -0.173
  6 07.48 .1047 -0.065
  7 49.38 .6013
  9 40.88 .5033
  9 49.38 .6913
 10 48,68 .6815
 11 46.28 .6479
 12 44.88 .6283
 13 26.19 .3665
 14 10.58 .1491
 15 30.38 .4252
```

TABLE IV OAL TEST 239-10 M = 2.00

```
p_x/p_{t,o} \Delta p/q
TAP
                                            Pic Rum Test
                            \alpha_{\mathbf{z}}
     \mathbf{p}_{\mathbf{x}}
PTO 71.43
                             16.0 -050.0 43 29 289-10
  1 06.88 .0963 -0.098
  2 06.18 .0865 -0.115
  4 05.48 .0767 -0.143
  5 06.28 .0879 -0.111
  6 07.38 .1033 -0.058
  7 49.13 .5885
  8 49.68 .6055
  9 49.08 .6871
 10 48.28 .6759
 11 45.48 .6367
 12 43.68 .5115
 13 27.98 .3917
 14 12.68 .1775
 15 35.58 .4981
PTO 71.38
                             16.0 -040.0 44 29 289-10
  1 06.88 .0964 -0.098
  2 06.78 .0950 -0.092
  4 03.98 .0559 -0.201
  5 04.08 .0572 -0.197
  6 06.88 .0964 -0.083
 7 48,68 .6820
8 49,69 .6946
9 48,68 .0820
 10 47.68 .6690
 11 44,58 .6301
 12 44.88 .6287
 13 42.28 .5923
 14 38.58 .5405
 15 23.88 .3345
PTO 71.38
                             16.0 -035.0 45 29 289-10
  1 06.98 .0979 -0.084
2 06.58 .0964 -0.088
  4 02.78 .0389 -0.243
  5 03.58 .0502 -0.217
6 06.88 .0964 -0.088
7 48.28 .6843
  8 49,48 .6932
  9 45 FR 6948
 10 47.78 .6694
 11 45.18 .6330
 12 45.88 .6428
 13 44.58 .6245
 14 44.38 .6217
 15 26.78 .3752
```

. ______

APPENDIX E (COMP'D)

TABLE IV OAL TRUE 289-10 M = 2.00

```
p_x/p_{t,0} \stackrel{\triangle}{=} p/q \quad \alpha_z
TAP
                                   ø
                                      Pic Run Test
     p_{\mathbf{x}}
PTO 71.23
                          20.0 +035.0 46 29 289+10
  1 06.28 .0832 -0.111
  2 06.68 .0938 -0.095
  4 02.98 .041P -0.240
  5 04.28 .0601 -0.100
  6 06.18 .0868 -0.115
  7 45.68 .6553
  0 47.28 .6630
  9 46.08 .6499
 10 45.18 .6343
 11 42.08 .5909
 12 42.88 .6020
 13 42.58 .5992
 14 41.48 .5823
 15 20.88 .2031
PTO 71.28
                          20.0 -040.0 47 29 289-10
  1 06.18 .0867 -0.115
  2 05.68 .0037 -0.005
  4 04,08 .0572 -0.307
  5 64,89 .0695 -7.166
  5 05.48 .0909 -0.105
  7 45.38 .6507
  8 47.18 .5619
  9 45.78 .6422
 10 44.09 .0134
 11 40.38 .5565
 12 41.88 .5075
 13 41.68 .5847
 14 40.28 .5651
 15 23.28 .3266
PTO 71.28
                          20.0 -030.0 49 29 290-10
 1 06.48 .0009 -0.103
  2 06.53 .0923 -0.009
 A 05.38 .0755 -0.3366
 5 05.38 .0755 -0.165
  5 05.08 .017% -1.00A
 7 48.08 .6465
 8 45.58 .6525
 9 46.28 .6212
 10 41.58 .5839
 11 34.68 .4565
 12 33.25 .4569
13 31.38 .4473
14 37.88 .5314
 15 25.13 .3533
```

TABLE IV OAL TEST 289-10 M = 2.00

```
p_x/p_{t,o} \triangle p/q
TAP
                                     ø
                                         Pic Run Test
     p_x
PTO 71.23
                            20.0 =055.0 49 29 289=10
  1 06.38 .0896 -0.107
  2 06,48 .0910 -0.103
  4 05.78 .0811 -0.130
  5 05.48 .0769 +0.142 6 06.69 .0936 +0.095
  7 46.48 .6525
  8 46.88 .6581
9 44.68 .6273
 10 41.29 .5795
 11 31.88 .4476
 12 25.88 .3633
 13 23.48 .3296
 14 23.68 .3324
 15 38.98 .5472
PTO 71.28
                           20.0 -060.0 50 29 239-10
  1 05.28 .0741 -0.350
  2 06.08 .0853 -0.119
  4 05.58 .0783 -0.138
  5 05.48 .0760 -0.142
  6 06.28 .0881 -0.111
  7 47.18 .0619
  8 47.48 .6661
  9 45.78 .6423
 10 42.98 .6030
 11 30.03 .4220
 12 20.68 .2001
 13 12.03 .1605
 14 15.28 .2144
 15 38,58 .5412
PTO 71.23
                           20.0 -065.0 51 29 290-13
  1 05.48 .0769 -0.142
  2 05.88 .0825 -0.127
  4 05.18 .0727 -0.154
6 06.00 .0854 -0.118
7 47.83 .6722
  8 49,08 .6750
 9 46.78 .6567
 10 44.78 .6287
 11 37.98 .5332
 12 21.48 .3016
 13 08.98 .1261
 14 14.48 .2033
 15 38.68 .5430
PTO 71.38
                           20.0 -076.0 52 29 289-10
```

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TABLE IV OAD TEST 289-10 N = 2.00

```
p_x/p_{t,o} \Delta p/q \alpha_{t,o}
TAP
                                 Ø Pic Run Test
     \mathbf{p}_{\mathbf{x}}
  1 05.48 .0768 -0.142
  2 05.48 .0768 -0.142
  4 05.18 .0726 -0.154
  6 05.38 .0824 -0.127
  7 48.68 .6920
  8 48488 46848
  9 47.88 .6708
 10 46.68 .6540
 11 40.38 .5657
 12 24.78 .3472
 13 11.98 .1678
 14 16.08 .225%
 15 38.58 .5405
PTO 71.53
                         20.0 -150.0 53 29 289-10
  1 09.08 .1269 -0.002
  2 08.68 .1213 -0.013
  4 03.88 .1381 0.729
  6 11.68 .163% 0.099
  7 44.98 .6220
 8 43.38 .6055
 9 43.88 .6134
 10 44.18 .6176
 11 41.89 .5855
 12 41.48 .5700
 13 39.88 .5575
 14 37.28 .5212
 15 22.68 .3171
PTO 71.43
                         20.0 -165.0 54 29 289-10
  1 00.18 .1295 0.002
  2 09.08 .1271 -0.002
  4 10.88 .1529 0.059
  6 12.60 .1803 0.347
  7 47.68 .6675
 8 45.15 .5465
 9 44,09 .6171
 10 44.28 .5199
 11 42.18 .5005
 12 40,48 .5667
 13 41.28 .5770
 14 39.68 .5555
 15 37.79 .5289
PTO 71.48
                         20.0 -180.0 55 29 209-10
  1 09.88 .1382 0.029
  2 09.28 .1298 0.006
```

TABLE IV OND TEST 289-10 N = 2.00

TAP	$p_{\mathbf{x}}$	$p_{x}/p_{t,c}$	_p /q	°×	ø	Pie R	m Test
6 7 8 9 10 11 12 13		.6866 .6670 .6726 .6517 .6349 .5990					
1		•1466 •1382		23•0	180.º	56 29	289 -1 0
6 7 8 9 10 11 12 13		.7146 .6950 .6712 .4810 .6628 .405 .6088 .5579	0.131 0.229				
3	71.53 09.83 09.78		0.025	23.0	~ 165•0	57 29	289-10
6 7 8 10 11 12 13	11.99 14.46 47.69 45.08 42.69 44.28 40.49 37.28 34.48 35.23	.2024 .6666 .6442 .6107 .6100 .5011 .5650 .5212	0.131				
1			0.002 0.002	23•0	-150.0	58 29	289-10
4	10.83	•1523	0.069				

APPRIDIX E (CONT'D)

TABLE IV OAL TEST 289-10 M = 2.00

```
TAP px
            p_x/p_{t,o} \Delta p/q \alpha_t
                                  Ø Pic Run Test
   6 12.98 .1817 0.151
   7 43.48 .6097
   8 41,48 .5907
   9 40.28 .5520
  10 42.08 .5891
  13 30.58 .5541
  12 38,78 .5420
  13 37.28 .5219
  14 34,68 .ABSE
  15 22.48 .3147
 PTO 71.48
                          23.0 -070.0 59 29 289-10
  1 05,68 .0705 -0.135
   2 06.18 .0965 -0.175
  4 05,68 40795 -0.125
  6 05.38 .0753 -0.147
   7 47.18 .6500
  8 47.38 .0628
  9 45,49 6363
  10 41,33 .6700
  11 22,43 .3145
 12 15.88 .2222
 13 11,09 .1676
 14 17,98 ,1962
 15 32,53 .4740
PTO 71.39
                          23.0 -065.0 60 29 280-10
  1 95.38 .0784 -0.146
  2 06.08 .0852 -0.170
  4 05.78 .0810 -0.121
  5 05.28 .0740 +0.150
  7 45.68 .5400
  8 45.88 .6428
  9 43.28 .6062
 10 31.49 .4410
 11 14.78 .2071
12 18.08 .2532
 13 10.30 .147
14 12,48 .1
 15 34,48 .48.
PTO 71.63
                         23.0 -060.0 61 20 380-10
 1 05.18 .0722 ~0.155
  2 06.68 .0033 -0.006
 4 05.88 .0821 -0.128
  6 05.28 .0737 -0.151
  7 44.28 .6132
```

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TABLE IV OAL TEST 289-EO H = 2.00

```
p_x/p_{t,o} \triangle p/q \quad \alpha_i
TAP
                                   ø
                                        Pic Run Test
     \mathbf{p}_{\mathbf{x}}
  8 44.08 .6154
  9 38.58 .5386
 10 30.28 .4227
 11 18.58 .2594
 12 17.78 .3432
 13 16.48 .2301
 14 13.68 .1910
 15 35.58 .4967
PTO 71.43
                          23.0 -055.0 62 29 289-10
  1 05.13 .0718 -0.156
  2 06.53 .0914 -0.102
  4 05.93 .0830 -0.125
  6 05.43 .0760 -0.145
  7 42.83 .5996
  8 42.53 .5969
  9 38413 +5338
 10 33,43 ,4680
 11 23.43 .3220
 12 23.23 .3252
 13 25.33 .3586
 14 25.12 .3519
 15 36.53 .5114
PTC 71.53
                          23.0 -050.0:53 29 289-10
 1 05.58 .0780 -0.139
  2 06.98 .0976 -0.024
  4 05.78 .0808 -0.131
  6 05.48 .0766 -0.143
  7 42,58 .5953
  6 43,18 .6037
 9 38,78 ,5422
 10 36.68 .5129
11 23.59 .3996
 12 30.18 .4219
 13 26.19 .3560
 14 35,88 ,5016
 15 27.60 .3370
PTO 71.58
                          23.0 -040.0 64 29 289-10
  1 05.98 .0835 -0.124
  2 07.18 .1002 ~0.077
  4 04.05 .0570 -0.103
  6 05.48 .0766 -0.143
 7 42.98 .6006
 8 43,28 .6046
  9 40.88 .5711
```

TABLE IV OAL TEST 289-10 14 = 2.00

```
p_{\chi}/p_{t,o} \Delta_{p/q}
                                     Ø Pic Run Test
                           \alpha_{\mathbf{g}}
TAP
     \mathbf{p}_{\mathbf{x}}
 10 39.78 .5557
 11 35.88 .5013
 12 38 18 .5334
 13 38.28 .5349
 14 36.78 .5139
 15 23.69 .3308
                             23.0 -135.0 65 29 289-10
PTO 71.53
   1 05.78 .0808 -0.131
   2 06.88 .0962 #0.088
  4 03.28 .0459 -0.229
   6 05.48 .0765 -0.143
  7 40.68 .5687
  8 42, 98 . 5995
  9 40.88 .5715
 10 40.08 .5603
11 37.28 .5212
12 39.18 .5477
 13 38.70 .5422
  14 36.78 .5142
 15 20.68 .2891
                             00.0 000.0 66 29 289-10
PTO 71.53
   1 00.08 .1260 ~0.002
   2 08,59 .1199 ~9.022
  4 08.68 .1247 -0.010
   6 09.00 .126° -0.002
7 49.88 .6973
   8 49.78 .6889
  9 40 68 .6045
  11 50.18 .7015
  12 50.18 .7015
  13 50.18 .7015
  14 50.29 .7043
  15 50.38 .7043
```

OAL 289-19

APPENDIX B

INDICATED TOTAL PRESSURE RATIOS FOR OAL TEST 289-19 H₀ = 2.00 Pt/Pt₁0

```
0.169 0.369 0.569 0.769 0.969
                                     Ø<sub>R</sub>
  00 .7082 .7038 .7067 .7169 ,7096
                                         000 1
                                    030
  04 .6990 .6976 .7063 .7165 .7107
  03 .6781 .6825 .6971 .7103 .7059
12 .6558 .6689 .6879 .6996 .6631
  16 •6022 •6285 •6052 •6402 •6504
  20 •4518 •5352 •5938 •6318 •6479
  23 •4251 •5304 •5977 •6372 •6548
 09 •7110 •7081 •7168 •7212 •7154 015 000 1
  04 •6976 •6976 •7092 •7180 •7121
 08 •6810 •6825 •6955 •7086 •7057
  12 •6510 •6582 •6728 •6902 •6902
 16 •5735 •6025 •6330 •6665 •6796
 20 .5273 .5579 .5855 .6059 .5826
 23 •4870 •5276 •5654 •5451 •5668
√00 .7101 .7072 .7072 .7101 .7188 000
                                         000 1
 04 .7014 .7000 .7087 .7087 .7233
 08 •6844 •6873 •6989 •7119 •7105
 12 .4582 .6432 .6679 .6912 .6927
 16 • 3872 • 6268 • 6297 • 6457 • 6558
√20 •3146 •5847 •5963 •6079 •6108
 23 •3291 •5353 •5469 •5556 •5484
 00 •7106 •7106 •7062 •7033 •7106 •015 000 1
 04 •7043 •7057 •7043 •7057 •7086
 08 .5730 .6936 .6979 .7052 .7052
 12 .2664 .5842 .6510 .6800 .7003
 16 .5332 .2132 .3965 .5768 .6422
 20 .3872 .5440 .4235 .4670 .5295
 23 •4750 •4750 •3441 •4095 •4459
 00 •7106 •7106 •7106 •7091 •7062 -030 000 1 1
 04 .7058 .7102 .7102 .7087 .7058
 08 •4380 •7008 •7052 •7052 •7037
 20 .5288 .1958 .1230 .2525 .4459
 23 •4357 •1696 •1478 •2525 •2525
 00 •7091 •7091 •7091 •7077 •7077 -040 000 1 1
 04 .7038 .7096 .7096 .7096 .7082
 08 .6078 .7082 .7111 .7111 .7096
 12 •6820 •6936 •7024 •7038 •7067
 16 .5695 .5303 .6306 .6699 .6830
 20 •5004 •2718 •2412 •3359 •5893
 23 •4501 •2313 •2138 •2445 •2911
 00 •7092 •7092 •7107 •7078 •7078 -045 000 1 1
 04 .7063 .7107 .7107 .7107 .7107
 08 •6947 •7107 •7136 •7136 •7121
 12 .6961 .7019 .7063 .7107 .7078
 16 .6-14 .6145 .6611 .6859 .6947
 20 •5019 •3533 •4218 •5252 •6490
```

```
INDICATED TOTAL PRESSURE RATIOS FOR OAL TEST 289-19 Mg = 2.00
           Pi/Pt.o
    0.169 0.369 0.569 0.769
                             0.969
23 •4640 •2732 •3140 •3140 •3461
00 .7395 .7095 .7080 .7051 .7037 -050 000 1
04 .7074 .7103 .7103 .7103 .7089
08 .7080 .7138 .7124 .7138 .7124
12 .6989 .7061 .7105 .7105 .7105
16 .6120 .6324 .6717 .6906 .6994
20 .5057 .3870 .5014 .6085 .6678
23 .4707 .2775 .3438 .4433 .5645
00 •7098 •7112 •7112 •7069 •7055 -055 000 1
04 •7084 •7112 •7127 •7112 •7098
08 •7134 •7163 •7163 •7149 •7105
23 •4741 •2780 •3550 •4741 •6078
00 •7115 •7130 •7130 •7101 •7086 -060 000 1 2
04 .7003 .7105 .7120 .7105 .7090
08 .7130 .7174 .7159 .7159 .7130
12 •7032 •7105 •7134 •7134 •7134
16 •6173 •5377 •6755 •6946 •7033
20 .5083 .3960 .5069 .6119 .6746
23 .4718 .2807 .3478 .4383 .5535
00 .7105 .7120 .7120 .7090 .7061 -065 000 1 2
04 •7116 •7131 •7131 •7131 •7116
08 .7116 .7160 .7160 .7160 .7160
12 •6975 •7048 •7077 •7106 •7091
16 .6080 .6226 .6649 .6897 .6970
20 .5032 .3615 .4170 .5076 .6523
23 .4657 .2820 .3140 .2849 .3126
00 .7110 .7110 .7110 .7096 .7067 -070 000 1 2
04 .7102 .7131 .7131 .7131 .7102
08 .6989 .7121 .7135 .7135 .7135
12 .6951 .7010 .7068 .7083 .7098
16 .5890 .5861 .6445 .6766 .6897
20 .5120 .3060 .2563 .3396 .6040
23 •4565 •2563 •2271 •2534 •2855
99 •7109 •7124 •7124 •7095 •7080 -075 000 1 2
04 .7061 .7119 .7104 .7119 .7104
09 .6421 .7120 .7120 .7134 .7120
12 .6780 .6925 .7012 .7041 .7070
16 .5640 .4038 .6077 .6630 .6819
20 .5047 .2337 .1740 .2701 .5455
23 •4478 •2147 •1914 •2395 •2759
00 •7101 •7115 •7130 •7086 •7072 -080 000 1 2
04 •7048 •7135 •7121 •7106 •7091
08 •5112 •7061 •7090 •7120 •7090
12 •5156 •6790 •6965 •7024 •7053
```

```
INDICATED TOTAL PRESSURE RATIOS FOR OAL TEST 289-19
                                                 N. = 2.00
            Pt/Pt.o
                                            è ma
      0.169 0.369 0.569 0.769
                              0.969
16 •5163 •2490 •4945 •6426 •6702
 2: .5312 .2070 .1285 .2463 .5399
 23 .4465 .1851 .1502 .2592 .2316
00 •7143 •7143 •7143 •7114 •7071 ~085 000 1
C4 • 7056 • 7143 • 7129 • 7114 • 7114
08 .4259 .7031 .7090 .7104 .7104
12 • 2894 • 6494 • 6828 • 6959 • 6988
16 •4393 •1880 •3739 •6180 •6586
20 .5406 .2053 .1515 .2662 .3794
23 •4535 •1719 •1936 •2227 •2532
00 .7114 .7129 .7129 .7100 .7071 -090 000 1 2
04 .7051 .7124 .7109 .7109 .7109
08 •4062 •6998 •7056 •7085 •7085
12 .2515 .6200 .6722 .6896 .6954
16 •4056 •1501 •3098 •5957 •6436
20 .5414 .2506 .2593 .3102 .4062
23 .4680 .1994 .3069 .2619 .3112
00 .7119 .7119 .7104 .7090 .7075 -095 000 1 2
C4 • 7056 • 7114 • 7114 • 7114 • 7114
08 .4309 .6969 .7042 .7071 .7085
12 .2523 .5898 .6581 .6814 .6901
16 •5185 •1533 •3221 •5621 •6276
20 •5418 •4588 •4065 •3948 •4559
23 •4872 •3313 •3284 •3429 •3677
00 •7150 •7150 •7150 •7120 •7105 -100 000 1 3
00 .7140 .7155 .7140 .7125 .7096
04 •7091 •7120 •7120 •7120 •7120
08 .5722 .7018 .7062 .7106 .7092
12 •2771 •5974 •6591 •6826 •6885
16 •5230 •2226 •3947 •5726 •6222
16 •5282 •1981 •3938 •5735 •6231
20 .4254 .5542 .4254 .4693 .5015
23 •5001 •5015 •3424 •4096 •4183
oc •7137 •7137 •7137 •7108 •7108 <del>•</del>105 000 1 3
04 .7079 .7108 .7108 .7122 .7108
79 •6450 •6962 •7020 •7049 •7049
12 •3130 •5901 •6435 •6747 •6806
16 •4201 •5121 •5034 •5910 •6202
20 •2876 •4953 •5129 •5304 •5451
23 •3679 •4340 •4560 •4736 •4707
90 •7147 •7147 •7118 •7104 •7060 <del>-110 000 1 3</del>
04 •7086 •7115 •7115 •7115 •7115
08 •6884 •6957 •7001 •7030 •7016
12 •3850 •6108 •6518 •6723 •6797
16 .2807 .5606 .5795 .6116 .6261
20 •3532 •4891 •5564 •5622 •5637
23 •3909 •4378 •4964 •5081 •5052
•00 •7153 •7153 •7123 •7109 •7065 -115 000 1 3
```

ı

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INDICATED TOTAL PRESSURE RATIOS FOR OAL TEST 289-19
                                                    K_ = 2.00
             Pé/Pto
                                              Par d
      0.169 0.369 0.569 0.769 0.969
04 .7091 .7105 .7120 .7120 .7105
08 •6907 •6966 •7009 •7038 •7009
12 •4440 •6347 •6582 •6758 •6787
16 .3794 .5980 .6083 .6259 .6317
20 .3378 .5678 .5722 .5810 .5795
23 .3780 .5213 .5125 .5257 .5183
00 .7153 .7153 .7138 .7123 .7065 -120 000 1 3
04 .7089 .7104 .7118 .7104 .7089
08 .6913 .6972 .7001 .7030 .7001
12 .3921 .6490 .6636 .6767 .6811
16 .3504 .6397 .6225 .6326 .6354
20 .3096 .5578 .5722 .5881 .5823
23 .3038 .5077 .5048 .5165 .5165
00 •7164 •7150 •7135 •7106 •7048 +125 000 1 3
04 .7087 .7087 .7087 .7087 .7058
08 .6902 .6946 .6990 .7019 .6990
12 .5506 .6553 .6640 .6757 .6830
16 .3271 .6271 .6271 .6315 .6432
20 .3562 .5194 .5252 .5514 .5645
23 • 3045 • 4840 • 4942 • 5293 • 5351
00 •7145 •7145 •7131 •7087 •7043 -130 000 1 3
94 .7072 .7086 .7086 .7072 .7043
C8 .6898 .6941 .6971 .6985 .7029
12 .6548 .6592 .6650 .6767 .6825
16 .4294 .5955 .6116 .6364 .6538
20 •5154 •5256 •5372 •5664 •5766
23 • 4585 • 4964 • 5110 • 5431 • 5460
00 •7151 •7136 •7092 •7092 •7063 -135 000 1 3
04 .7063 .7092 .7078 .7063 .7063
08 .6864 .6923 .6952 .6967 .7011
12 •6552 •5596 •6655 •6728 •6801
16 .5793 .5925 .6115 .6377 .6553
23 •5768 •5417 •5505 •5754 •5476
23 •5063 •5063 •5223 •5150 •5253
60 •7142 •7142 •7113 •7084 •7084 +150 000 1 3
04 .7041 .7070 .7070 .7041 .7070
08 .6816 .6899 .6933 .6948 .6977
12 .6611 .6670 .6728 .6816 .6479
16 •6074 •6191 •6308 •6045 •6220
24 •5429 •4931 •5400 •5839 •6074
23 •5748 •4785 •5297 •5825 •6030
```

INDICATED TOTAL PRESSURE RATIOS FOR OAL TEST 289-19 $V_0 = 2.00$

```
1.169 1.369 1.569 1.769
                               1.969
  00 .7038 .7038 .7038 .7038 .7009
                                      030
                                            000 1
                                                   1
  04 .7049 .7034 .7034 .7019 .7019
 DR .6936 .6957 .6942 .6942 .6957
 12 •6660 •6733 •6806 •6850 •6894
  16 .6577 .6679 .6767 .6825 .6884
  20 .6596 .6714 .6891 .6889 .6948
  23 .5694 .6796 .6870 .6972 .7016
  00 .7096 .7096 .7096 .7096 .7067
                                      015 000 1
  04 .7078 .7092 .7078 .7063 .7649
  08 .7014 .7028 .7014 .6999 .6970
  12 •6888 •6931 •6917 •6757 •6771
 16 •6272 •6360 •646] •3548 •6607
20 •5957 •6131 •6248 •6379 •6437
  23 .5900 .6046 .6162 .6307 .6365
√ 00 .7115 .7072 .7043 .7014 .7014
                                      000 000 1
 04 .7116 .7073 .7073 .7043 .7029
 08 .7076 .7032 .7047 .7018 .7018
 12 •6927 •6912 •6927 •6956 •6956
16 .6616 .6733 .6791 .6805 .6820
20 .6195 .6355 .6224 .6311 .6021
  23 .5542 .5658 .5760 .5556 .5658
 00 •7120 •7135 •7077 •7033 •6990 -015 000 1 1
 94 •7188 •7144 •7°86 •7043 •7014
 09 •7154 •7125 •7081 •7037 •7008
 12 .7018 .7018 .7003 .6960 .6974
 16 .6640 .6728 .6757 .6844 .6902
 20 .5745 .6021 .6195 .6428 .6558
 23 •4793 •5201 •5506 •5826 •6146
  10 •7019 •6975 •7019 •7019 •7004 =030 000 1 1
 64 • 7043 • 7029 • 7073 • 7058 • 7087

    • 7052 • 7067 • 7067 • 7081 • 7168

 12 •7019 •7048 •7125 •7150 •7135
 16 .6310 .7014 .7028 .7043 .7101
 20 •6233 •6524 •6684 •6860 •6844
 23 •3485 •6201 •6379 •6510 •6582
 CU •7648 •7033 •7004 •6975 •6960 -040 000 1
  74 •7182 •7067 •7053 •7024 •7024
 08 • 7095 • 7067 • 7053 • 7053 • 7053
 12 .7067 .7067 .7053 .7053 .7111
 16 •6017 •7004 •7062 •7091 •7106
 20 •5636 •6825 •6971 •7014 •7043
 23 •5420 •6543 •6747 •6820 •6849
 00 •7049 •7034 •7034 •7019 •7005 <del>-</del>045 000 1
 7078 •7107 •7002 •7078 •7078 •7078
 $8 •7107 •7107 •7092 •7092 •7092
 12 •7107 •7107 •7092 •7107 •7136
 16 .6990 .7034 .7092 .7092 .7092
 20 •6810 •6941 •7000 •7014 •7029
```

```
INDICATED TOTAL PRESSURE RATIOS FOR OAL TEST
                                             -9-19
                                                   M_0 = 2.00
            Pt/Pt,0
                                                   Æ
    1.169 1.369 1.569 1.769
                               1.969
                                      ø,
23 •5936 •6752 •6883 •6971 •6985
00 •7022 •7022 •7008 •6993 •6979 -050 000 1
04 .7074 .7074 .7060 .7060 .7060
08 •7124 •7109 •7109 •7109 •7109
12 • 7134 • 7120 • 7120 • 7134 • 7163
16 .7037 .7081 .7125 .7139 .7139
20 •6910 •7011 •7026 •7040 •7055
23 •6568 •6856 •6943 •6957 •6986
00 •7040 •7026 •7026 •7011 •6997 <del>-</del>055 000 1
04 •7098 •7098 •7084 •7084 •7084
08 •7120 •7120 •7120 •7120 •7134
12 • 7149 • 7134 • 7134 • 7149 • 7192
16 .7134 .7149 .7163 .7178 .7178
20 .7120 .7120 .7192 .7192 .7178
23 .6804 .6949 .7080 .7080 .7037
00 •7072 •7057 •7057 •7043 •7043 •060 000 1
04 .7105 .7105 .7076 .7076 .7076
08 •7145 •7130 •7130 •7130 •7145
12 • 7134 • 7134 • 7134 • 7134 • 7178
16 .7077 .7106 .7164 .7179 .7179
20 .6965 .7038 .7082 .7097 .7097
23 .6586 .6849 .6922 .6951 .6965
09 .7047 .7047 .7032 .7018 .7032 -065 000 1
04 .7131 .7131 .7116 .7087 .7087
08 .7146 .7146 .7131 .7116 .7131
12 .7106 .7106 .7121 .7135 .7150
16 • 7043 • 7073 • 7121 • 7160 • 7175
20 .6844 .6932 .7005 .7019 .7049
23 •5925 •6654 •6829 •6858 •6887
00 .7037 .7037 .7037 .7023 .7008 -070 000 1
04 •7131 •7116 •7116 •7087 •7087
08 •7135 •7121 •7106 •7106 •7121
12 •7127 •7127 •7127 •7171
16 .6985 .7029 .7116 .7116 .7116
20 .6683 .6800 .6917 .6961 .6975
23 •5470 •6391 •6683 •6742 •6800
36 .7080 .7066 .7051 .7022 .7022 -075 000 1 2
04 •7104 •7090 •7090 •7075 •7075
09 •7134 •7120 •7134 •7134 •7149
12 •7099 •7084 •7099 •7142 •7157
16 •6936 •7008 •7067 •7067 •7096
20 .6460 .6635 .6780 .6824 .6897
23 •5440 •6168 •6518 •6635 •6722
00 •7043 •7043 •7043 •7028 •7013 <del>•</del>080 000 1 2
94 •7196 •7106 •7091 •7077 •7077
08 •7120 •7120 •7105 •7090 •7134
12 • 7082 • 7082 • 7140 • 7140 • 7111
```

1.

```
INDICATED TOTAL PRESSURE PATIOS FOR OAL TEST 289-19
               Pi/Puo
y 1.169 1.369 1.569 1.769 '1.969
                                      P<sub>R</sub>
 16 .6877 .6964 .7022 .7022 .7037
 20 .6242 .6446 .6649 -6766 .6853
 23 •3536 •5947 •6310 •6441 •6586
 00 .7056 .7071 .7056 .7027 .7013 -085 000 1
 04 .7100 .7100 .7085 .7085 .7056
 08 .7104 .7090 .7090 .7075 .7104
 12 .7046 .7046 .7046 .7075 .7090
 16 •6761 •6848 •6935 •6993 •7022
 20 •5841 •6204 •6523 •6640 •6756
 23 .3635 .4811 .5885 .6204 .6407
 00 •7071 •7071 •7056 •7027 •6984 -090 000 1 2
 04 .7169 .7080 .7080 .7051 .7022
U8 .7085 .7085 .7056 .7042 .7056
 12 .6997 .6997 .7012 .7055 .7099
16 .6669 .6727 .6930 .6959 .7017
 20 •5283 •598] •6417 •6562 •6707
 23 •3853 •4665 •5594 •5914 •6291
 00 .7061 .7046 .7017 .6973 .6944 -095 000 1 2
 P4 .7100 .7056 .7027 .6998 .7027
 48 .7071 .7042 .7027 .7056 .7056
 12 •6945 •6930 •7003 •7018 •7032
 16 .6552 .6669 .6814 .6916 .7003
 20 .5418 .5854 .6319 .6509 .6712
 23 44304 4945 45513 45964 46256
 99 •7991 •7061 •7032 •7061 •7047 -100 000 1
 NO .7096 .7067 .7037 .7052 .7037
 54 •7105 •7076 •7061 •7076 •7076
 13 •7092 •7077 •7106 •7121 •7136
 12 .6944 .7017 .7091 .7091 .7091
 16 .3602 .6704 .6879 .6937 .7010
 16 .6597 .6699 .6885 .6933 .7020
 20 .5689 .6069 .6391 .6552 .6714
 23 •4767 •5001 •5789 •5993 •6285
 00 •7064 •7049 •7049 •7020 •6991 -105 000 1 3
 4 •7079 •7035 •7049 •7049 •7035
 08 .7020 .7035 .7049 .7035 .7035
 12 •6879 •6932 •6952 •6966 •7025
 16 .6524 .6611 .6786 .6874 .6918
    •5875 •6006 •6358 •6504 •6665
 23 •5148 •5265 •5588 •5764 •6028
 00 •7030 •7016 •7045 •7001 •6987 -110 000 1 3
 04 •7056 •7086 •7086 •7056 •7042
 ·* •7001 •7045 •7045 •7030 •7074
 12 .6399 .6914 .6958 .7002 .7002
 16 •6538 •6626 •6801 •6859 •6874
 20 •6104 •6207 •6455 •6499 •6689
 23 •5404 •5463 •5741 •5756 •5932
 00 •7636 •7665 •7065 •7036 •7065 -115 000 1 3
```

1

```
INSIGATED TOTAL PRESSURE RATIOS FOR OAL TEST 289-19 No = 2.00
            PL/PL,0
v 1.169 1.369 1.569 1.769 1.969
                                    Ø,
04 • 7061 • 7091 • 7091 • 7061 • 7091
08 .7024 .7053 .7038 .7082 .7053
12 •6904 •6919 •6963 •6992 •6992
16 .6552 .6655 .6846 .6816 .6875
20 .6103 .6250 .6543 .6367 .6045
23 .5476 .5505 .5783 .5768 .5710
00 •7050 •7079 •7079 •7094 •7065 -120 000 1
04 •7089 •7104 •7089 •7147 •7089
08 .7060 .7060 .7060 .7089 .7045
20 .5895 .5996 .5270 .5953 .6155
23 .5572 .5674 .5543 .5660 .5878
00 •7077 •7077 •7077 •7106 •7048 -125 000 1
04 •7102 •7116 •7087 •7116 •7073
08 •7048 •7048 •7106 •7077 •7033
12 •6902 •6931 •7004 •6960 •6931
16 .6679 .6738 .6898 .6388 .6534
20 •5980 •5966 •5980 •6082 •6271
23 .5701 .5497 .5760 .5877 .6081
00 •7087 •7087 •7145 •7087 •7058 +130 000 1
04 .7086 .7086 .7144 .7101 .7057
08 •7043 •7058 •7087 •7029 •7014
12 .6912 .6912 .6985 .6927 .6796
16 .6772 .6393 .6422 .6451 .6597
20 •5795 •5897 •6116 •6203 •6393
23 •5489 •5722 •5985 •6101 •6276
00 .7078 .7092 .7136 .7092 .7063 -135 000 1
04 .7092 .7092 .7136 .7092 .7063
08 •7040 •7040 •7055 •7011 •6996
12 .6889 .6889 .6918 .6743 .6772
16 •6173 •6319 •6480 •6524 •6640
20 •5856 •6861 •6265 •6338 •6528
23 •5735 •5939 •6173 •6275 •6465
00 .7084 .7084 .7142 .7084 .7055 -150 000 1
04 .7085 .7099 .7143 .7070 .7041
08 •6992 •6992 •7036 •6977 •6962
12 •6626 •6714 •6816 •6831 •6875
16 •6455 •6601 •6748 •6748 •6865
20 •6396 •6572 •6704 •6748 •6894
23 •6396 •6572 •6748 •6777 •6953
```

INDICATED TOTAL PRESSURE RATIOS FOR OAL TEST 289-19 Mo = 2.00 Pt/Pt.o

```
Bake
   2.169 2.369 2.569 2.769 2.969
                                           ø
                                     g_{\mathbf{R}}
                                          000 1
00 .7009 .6995 .6980 .6966 .6951
                                     930
04 •7019 •7005 •7005 •6990 •6976
08 •6971 •7000 •7000 •7000 •7000
12 .6938 .6981 .7011 .7025 .7055
16 .5957 .6986 .7059 .7103 .7146
20 .7006 .7065 .7138 .7211 .7241
23 .7089 .7133 .7206 .7279 .7308
00 .7052 .7037 .7023 .6994 .6965
                                    015 000 1 1
04 .7034 .7019 .7005 .6961 .6961
08 .6941 .6941 .6941 .6926 .6912
12 •6800 •6815 •6844 •6859 •6888
16 •6665 •6694 •6766 •6825 •6868
20 •5539 •6597 •5684 •6786 •6830
23 •6481 •6539 •6641 •6742 •6800
00 .6999 .6999 .6970 .6941 .6897
                                    000 000 1
04 .7014 .7000 .6956 .6927 .6912
08 .7003 .6974 .6931 .6902 .6887
12 •6927 •6898 •6839 •6810 •6825
16 •6805 •5573 •5631 •6645 •6674
20 •6166 •6239 •6340 •6428 •6515
23 •5847 •5934 •6064 •6210 •6326
00 .6975 .6960 .6946 .6931 .6902 -015 000 1 1
04 .6999 .6984 .6970 .6941 .6912
08 • 7008 • 7008 • 6994 • 6979 • 6950
12 •6989 •6989 •6974 •6974 •6974
16 •6931 •6946 •6975 •7004 •6990
20 .6718 .6791 .6878 .6936 .6936
23 •6437 •6524 •6640 •6757 •6786
00 •7091 •7062 •7019 •6975 •6931 -030 000 1
04 .7160 .7102 .7058 .7043 .7014
18 •7139 •7110 •7139 •7125 •7067
12 •7135 •7164 •7135 •7091 •7077
16 .7115 .7072 .7043 .7072 .7072
20 •6873 •6873 •6902 •6960 •6975
23 •6640 •6699 •6742 •6815 •6830
00 •6946 •6931 •6902 •6888 •6931 -040 000 1
04 •6995 •6980 •6995 •7053 •7038
08 .7038 .7111 .7126 .7111 .7082
12 •7140 •7140 •7126 •7184 •7198
16 .7208 .7208 .7179 .7179 .7179
20 •7058 •7058 •7058 •7073 •7073
23 •6893 •6908 •6908 •6952 •6952
00 .6990 .6976 .6961 .6961 .6961 -045 000 1 1
04 .7049 .7049 .7078 .7049 .7005
08 .7121 .7136 .7121 .7107 .7078
12 .7121 .7107 .7092 .7092 .7078
16 •7121 •7121 •7107 •7121 •7121
23 •7073 •7145 •7131 •7174 •7174
```

.

INDICATED TOTAL PRESSURE RATICS FOR OAL TEST 229-19 Mg = 2.00 PL/Pt.o

```
øs
   2.169 2.369 2.569 2.769 2.969
                                   An
23 .7014 .7029 .7029 .7058 .7073
00 .6964 .6964 .6964 .6935 .6935 -050 000 1 2
04 .7045 .7031 .7045 .7060 .7031
08 •7136 •7153 •7138 •7124 •7109
12 .7163 .7149 .7134 .7134 .7120
16 .7125 .7110 .7081 .7081 .7081
20 .7084 .7084 .7069 .7098 .7127
23 .7000 .7000 .7000 .7044 .7087
00 -6997 -6982 -6982 -6997 -6997 -055 000 1 2
04 .7069 .7069 .7112 .7098 .7040
08 .7149 .7178 .7163 .7149 .7134
12 •7192 •7178 •7163 •7149 •7149
16 • 7178 • 7163 • 7134 • 7149 • 7149
20 .7163 .7120 .7076 .7076 .7076
23 .7066 .7066 .7037 .7066 .7066
00 .7013 .6999 .6970 .6970 .6970 -060 000 1 2
04 •7061 •7047 •7061 •7061 •7047
08 .7159 .7159 .7159 .7159 .7130
12 •7192 •7192 •7163 •7134 •7134
16 •7179 •7164 •7135 •7150 •7150
20 .7326 .7126 .7111 .7111 .7111
23 .6980 .6994 .6965 .7009 .7038
** .7018 .6989 .6960 .6960 .6960 -065 000 1 2
04 .7087 .7087 .7087 .7087 .7058
08 .7160 .7189 .7175 .7160 .7146
12 •7164 •7164 •7150 •7135 •7135
16 • 7189 • 7160 • 7131 • 7131 • 7131
20 .7063 .7063 .7049 .7063 .7063
23 •6916 •6931 •6916 •6975 •7019
00 •6994 •6979 •6979 •6965 •6965 -070 000 1 2
04 • 7087 • 7087 • 7102 • 7087 • 7043
08 •7150 •7150 •7150 •7121 •7091
12 •7171 •7171 •7156 •7156 •7127
16 •7116 •7116 •7087 •7102 •7102
20 .6990 .6990 .6990 .7034 .7034
23 •6859 •6873 •6859 •6917 •6961
00 .7022 .7008 .7008 .7022 .6993 -075 000 1
64 .7075 .7075 .7090 .7075 .7031
08 •7149 •7149 •7134 •7120 •7090
12 •7128 •7099 •7070 •7070 •7070
16 • 7081 • 7067 • 7067 • 7096 • 7081
20 .6955 .6955 .6959 .7013
23 •6780 •6809 •6809 •6853 •6926
00 •6999 •6984 •6999 •6999 •6955 ←080 000 1
04 .7077 .7091 .7077 .7033 .6989
08 .7120 .7090 .7061 .7061 .7061
12 •7082 •7082 •7111 •7082 •7082
```

```
INDICATED TOTAL PRESSURE RATIOS FOR OAL TEST 289-19
                                                 M_{\Lambda} \approx 2.00
           Pt/Pto
a<sub>1</sub>\ 2.169 2.369 2.569 2.769 2.969
                                     P<sub>R</sub>
                                                 Ting.
16 .7080 .7066 .7051 .7051 .7051
20 .6896 .6911 .6911 .6984 .6998
23 .6673 .6732 .6761 .6819 .6833
00 •6998 •6969 •6969 •6940 •6925 •085 000 1
04 .7071 .7056 .7027 .7027 .6998
#8 .7075 .7194 .7104 .7075 .7046
12 •7104 •7104 •7090 •7075 •7061
16 .7051 .7051 .7037 .7109 .7080
20 •6814 •6901 •5886 •6930 •6930
23 .6582 .6611 .6611 .6698 .6756
00 .6954 .6925 .6954 .6940 .6940 -090 000 1
04 .7008 .7037 .7051 .7022 .6993
"8 •7085 •7085 •7085 •7071 •7035
12 .7099 .7099 .7070 .7128 .7084
16 • 7046 • 7104 • 7061 • 7061 • 7031
20 .6838 .6853 .6824 .6911 .6940
23 •6436 •6494 •6552 •6669 •6727
00 .6988 .6959 .6959 .6930 .6930 -095 000 1
04 .7027 .7013 .6098 .7027 .7027
08 •7056 •7056 •7129 •7085 •7027
12 • 7061 • 7120 • 7090 • 7047 • 7018
16 .7076 .7032 .7003 .7032 .7003
20 .6800 .6814 .6829 .6916 .6945
23 •6402 •6489 •6562 •6693 •6751
00 .7032 .7032 .7047 .7032 .6973 ~100 000 1
00 .7022 .7008 .7037 .7022 .6964
04 .7091 .7091 .7105 .7032 .6973
₹8 •7136 •7136 •7077 •7048 •7018
12 •7105 •7061 •7032 •7032 •7003
16 .7010 .6995 .6966 .6981 .6952
16 .7020 .6991 .6976 .6991 .6962
20 .6772 .6831 .6860 .6933 .6889
23 •6460 •6563 •6621 •6723 •6752
30 •6976 •7020 •6962,•6918 •6889 ~105 000 1
04 .7049 .7020 .6976 .6933 .6903
08 •7064 •7020 •6991 •6976 •6962
12 •6995 •6981 •6966 •6981 •6952
16 •6918 •6933 •6933 •6933 •6845
20 .6767 .6884 .6796 .6489 .6504
23 •6205 •5852 •5926 •6073 •6146
00 •7030 •6987 •6943 •6928 •6884 ~110 000 1 3
^4 •7)56 •6998 •6998 •6953 •6909
08 .7030 .7001 .6972 .6913 .6884
12 •6059 •6943 •6899 •6870 •6841
16 •6859 •6859 •6772 •6684 •6728
20 •6762 •6207 •6324 •6426 •6455
23 •5741 •5946 •6020 •6166 •6210
00 •7006 •6962 •6948 •6918 •6889 •115 000 1 3
```

INDICATED TOTAL PRESSURE RATIOS FOR OAL TEST 229-19 $M_0 = 2.00$ Pt/Pt.o

```
2.169 2.369 2.569 2.769 2.969
                                     p_{\mathbf{R}}
04 •7032 •7003 •6973 •6944 •6885
08 •7009 •6980 •6951 •6893 •6849
12 •6963 •6919 •6846 •6831 •6816
16 •6846 •6582 •6611 •6655 •6714
20 •6162 •6279 •6367 •6469 •6513
23 •5856 •6031 •6090 •6236 •6280
00 .7006 .6977 .6948 .6918 .6889 -120 000 1
04 .7030 .6987 .6972 .6928 .6884
08 •7001 •6972 •6928 •6884 •6840
12 •6927 •6840 •6781 •6811 •6796
16 .6512 .6555 .6598 .6670 .6698
20 •6242 •6357 •6415 •6545 •6588
23 •6009 •6155 •6213 •6344 •6373
00 • 7033 • 7004 • 6990 • 6960 • 6931 - 125 000 1
04 •7058 •7014 •6971 •6941 •6883
08 •7019 •6960 •6902 •6873 •6844
12 •6844 •6815 •6786 •6800 •6800
16 •6563 •6621 •6650 •6708 •6738
20 .6344 .6446 .6475 .6592 .6650
23 .6198 .6314 .6373 .6490 .6519
00 •7029 •7014 •7000 •6956 •6912 -130 000 1 3
04 .7028 .7014 .6984 .6955 .6897
08 •7000 •6941 •6927 •6912 •6883
12 •6810 •6825 •6825 •6839 •6839
16 •6626 •6699 •6713 •6772 •6786
20 •6466 •6538 •6568 •6655 •6684
23 •6364 •6466 •6509 •6640 •6655
00 .7034 .7019 .7005 .6976 .6917 -135 000 1 3
04 • 7034 • 7019 • 6990 • 6947 • 6917
08 •6967 •6938 •6938 •6923 •6923
12 •6801 •6831 •6860 •6875 •6875
16 •6684 •6757 •6786 •6845 •6859
20 •6587 •6674 •6689 •6791 •6791
23 •6524 •6626 •6640 •6757 •6786
00 •7025 •6996 •6981 •6938 •6908 -150 000 1 3
04 •7026 •7011 •7011 •6982 •6953
08 •6948 •6962 •6977 •6977 •6962
12 •6904 •6934 •6963 •6992 •7022
16 •6894 •6953 •6997 •7070 •7070
20 •6924 •7011 •7041 •7129 •7129
23 •6982 •7055 •7070 •7158 •7129
```

ړ.

INDICATED TOTAL PRESSURE RATIOS FOR OAL TEST 289-19 No = 2.00 PE/Pt.o

4/2	3.169	3.369	$p_{\mathbf{R}}$	ø	Sake	urg:
00 04 08 12 16 20 23	.6932 .7000 .7084 .7161 .7255	•6971 •7084	030	000	1	1
00 04 08 12 16 20 23		•6844 •6897 •6917 •6926 •6873	015	000	1	1
00 94 08 12 16 20 23	•6839 •6854 •6858 •6796 •6689 •6529 •6340	•6796 •6844 •6810 •6747 •6645	000	000	1	1
00 04 08 12 16 20 23	•6844 •6868 •6892 •6960 •6946 •6805 •6699	•6796 •6892 •6902 •6902	- 015	000	1	1
08 12 16	•6917	•6873 •6854 •6965 •7048 •7028 •6990 •6873	-030	000	1	1
	•6980 •7053 •7198 •7120 •7000	•6902 •6893 •7126 •7184 •7120 •7000 •6908	-040	000	1	1
00 04 08 12 16 20	•6961 •7034 •7063 •7092	.6874 .6888 .7019 .7092 .7092	- 045	000	1	1

INDICATED TOTAL ARRESTRE RATIOS FOR OAL TEST 289-19 Un = 2.00

1	ndicates	and Schil Lated C	PATTES FOR	CAL 1EST	239-	-14	M _O = 2.
	P±'/F					Ş	_ EI
a ₁	3.169	3.369		$p_{\mathbf{R}}$	ø	E E	B
23	•6971	•6971					
04 08 12 16	•6973 •7095	•7066 •7076 •7052		-050	000	1	2
00 04 08 12 16 20 23	.6997 .7105 .7134 .7105	.6895 .6924 .7076 .7120 .7105 .7047		- 055	000	1	2
00 04 08 12 16 20 23	.5989 .7171 .7120 .7121	•6911 •6930 •7057 •7120 •7106 •7067 •6965		-060	000	l	2
00 04 08 12 16 20 23	•7014 •7116 •7121 •7087	•6887 •6956 •7087 •7121 •7037 •6900		-065	000	1	2
00 04 08 12 16 20 23	.7077 .7083 .7058	.6877 .6941 .7048 .7068 .7073 .7075		-070	000	1	2
09 08 12 16 20 23	•6973	.6906 .6901 .7018 .7041 .7037 .6999		- 075	000	1	2
00 04 08 12	•6897 •6931 •7047 •7067	•6868 •6873 •7003 •7053		- 080	000	1	2

1	IDICATI PE/	D TOTAL	PRESSURE	RATIOS	Por	OAL TES	T 2 89	-19	H _o = 2.00
	•	3.369		•		4	ø	Ä	5
a ₁ /y	3,109	70707		:		$p_{\mathbf{R}}$	p	Ã	Rus
16	.7051	•7066							
	6954								
23	.6790								
	• • • • •								
	. 6882					-085	000	1	2
C 4									
	•7031								
	.7090								
16	•7022 •6930								
23	•6756								
2. 2	•0725	•0110							
0.0	•6882	•6867				-090	000	1	2
04	.6935	•6906							
-08	•7056	•6969							
12	7941	•6997							
	•6988								
	•6940								
23	•6756	•6785							
0.0	•6915	•6901				-095	000	7	2
04							00	*	_
08									
12	.6989	•6945							
16									
20									
23	• 6766	•6751							
00	.6885	.6856				-100	000	1	3
0.0	•6875	•6861				_		•	_
04	•6914	•68 7 0							
98									
12	• 6959								
16									
16	•6903								
20	•6831								
23	•6519	•0313							
00	.6830	.6845				-105	000	1	3
04	.6874								
Bei	•6903	∙6859							
12	6893	•6835							
16									
20	•6562								
23	•6234	•6293							
00		•6826				-110	000	1	3
34							-	-	-
08	•6855		•						
12		•6841							
16	•6728								
5.0	•6528								
23	•6313	•6342							
0.0	•6816	•6831				-115	000	1	3

1			PRESSUR E	RATIOS	FĆR	OAL TEST	289	-19	Po = 2.00
	P\$/	Pt,o							•
aj/	3.169	3.369				\mathbf{z}_{R}	ø	Bak	Run
04									
	•6835								
12		6846							
16	6758								
20 23	•6572 •6382	•66∩] •6411							
25	• 0502	•0411							
00	•6816	•6831				-120	000	1	3
04		◆6767							_
08									
12									
16									
20	•6660								
23	•6475	•6505							
00	.6844	.6844				-125	000	1	3
04	•6825					145	000	1	5
0.8									
12	•6815	•6930							
16	•6796	•6825							
20									
23	•6606	•6636							
00	•6854	•6883				-130	000	3	3
34									•
08	• 6869								
12	•6869								
16	. 6844								
2.0	•6801								
23	•6757	•6772							
	•6859	•6859				-135	000	1	3
0.4	◆6888						_	_	_
0.8	• 6908								
12	6918								
16		•6933							
20	•6879								
۷)	•6903	• 6418							
00	.6864	•6879				-150	000	1	3
04	• 6924	•6894						-	_
	•6977	•6948							
12	• 7051	•7051							
16	•7158	•7158							
20 23	•7217 •7246	•7217 •7275							

INDICATED TOTAL PRESSURE RATIOS FOR OAL TEST 289-19 H₀ = 2.00 Pt/Pt₀

```
0.069 0.269 0.469 0.669 0.869
                                    p_{\mathbf{R}}
00 .7082 .7082 .7067 .7067 .7038
                                   030 000 5
04 .7034 .7034 .7019 .7019 .7005
08 .6971 .6971 .6986 .6986 .7000
12 .7084 .7098 .7128 .7142 .7157
16 • 7307 • 7336 • 7380 • 7409 • 7438
20 .7563 .7694 .7782 .7797 .7811
23 .7806 .7996 .8084 .8084 .8084
00 •7110 •7125 •7096 •7096 •7067 015 000 5
04 •7063 •7063 •7049 •7034 •7034
08 •7101 •7086 •7072 •7072 •7057
12 .7324 .7280 .7237 .7222 .7222
16 .7609 .7551 .7537 .7537 .7537
20 .7862 .7949 .7964 .7920 .7920
23 .8135 .8251 .8251 .8208 .8193
00 .7072 .7072 .7072 .7086 .7072
                                  000 000 5
04 .7058 .7058 .7029 .7029 .7029
08 •7148 •7119 •7105 •7076 •7090
12 • 7393 • 7349 • 7291 • 7247 • 7247
16 .7676 .7618 .7589 .7575 .7575
20 • 7909 • 8010 • 7996 • 7952 • 7938
23 .8228 .8330 .8286 .8228 .8199
00 •7077 •7062 •7048 •7048 •7048 -015 000 5
04 • 7043 • 7043 • 7028 • 6999 • 6999
08 .7067 .7081 .7067 .7052 .7037
12 .7279 .7294 .7250 .7221 .7207
16 • 7542 • 7542 • 7528 • 7528 • 7528
20 .7764 .7923 .7909 .7865 .7865
23 .8037 .8226 .8197 .8168 .8124
00 .7077 .7062 .7048 .7033 .7019 -030 000 5
04 .7014 .7014 .7014 .7000 .7000
08 .6921 .6979 .6979 .6994 .6994
12 .7004 .7120 .7106 .7106 .7106
16 .7159 .7333 .7319 .7333 .7362
20 .7309 .7644 .7659 .7673 .7673
23 .7484 .7920 .7935 .7935 .7906
00 .7062 .7062 .7033 .6990 .6975 -040 000 5 1
04 •6995 •6995 •6966 •6936
08 •6791 •6878 •6907 •6907 •6907
12 •6733 •6966 •6980 •6980 •6980
16 •6815 •7120 •7135 •7179 •7208
20 •6898 •7364 •7437 •7480 •7509
23 •6995 •7623 •7666 •7710 •7798
00 .7063 .7078 .7019 .6961 .7049 -045 000 5 1
04 .6990 .7005 .6976 .6932 .6932
08 •6713 •6830 •6844 •6844 •6844
20 •6592 •7174 •7247 •7335 •7451
```

```
INDICATED TOTAL PRESSURE RATIOS FOR OAL TEST 289-19 N = 2.00
            Pé/Pt.0
0.069 0.269 0.469 0.669 0.869
                                    \phi_{\mathbf{R}}
23 .6636 .7378 .7451 .7611 .7670
00 .7037 .7037 .7008 .6949 .7008 -050 000 5 2
04 .6987 .6987 .6973 .6915 .6944
08 .6688 .6790 .6819 .6804 .6833
12 .6392 .6741 .6800 .6843 .6887
16 .6324 .6819 .6863 .6950 .7081
20 .6316 .6982 .7098 .7257 .7359
23 .6308 .7159 .7274 .7491 .7620
00 .7055 .7055 .6997 .6982 .7069 -055 000 5 2
04 •6968 •6997 •6982 •6939 •7011
08 .6683 .6741 .6770 .6756 .6872
12 .6203 .6625 .6683 .6756 .6887
16 46058 46640 46727 46858 47003
20 .5999 .6756 .6901 .7149 .7338
23 .5933 .6906 .7066 .7313 .7501
00 .7072 .7072 .7028 .7086 .7174 -060 000 5 2
04 .6930 .6960 .6945 .7018 .7105
08 .6664 .6780 .6766 .6839 .6941
12 •6014 •6494 •658] •6741 •6872
16 .5808 .6479 .6581 .6800 .7004
20 .5696 .6528 .5703 .6994 .7199
23 .5579 .6644 .6849 .7155 .7345
00 .7047 .7047 .7003 .7090 .7163 -065 000 5 2
04 •6927 •6970 •6956 •7058 •7131
08 .6635 .6766 .6795 .6868 .6956
12 .5721 .6290 .6421 .6639 .6814
16 .5481 .6255 .6401 .6664 .6868
20 .5310 .6245 .6479 .6815 .7019
23 .5167 .6333 .6639 .7048 .7150
00 .7037 .7037 .7067 .7168 .7139 -070 000 5 2
04 .6927 .6970 .6985 .7116 .7116
08 .6596 .6742 .6756 .6887 .6916
12 .5562 .6162 .6308 .6571 .6747
16 .5160 .6021 .6211 .6532 .6737
20 .4959 .5982 .6289 .6727 .6844
23 .4784 .6026 .6391 .6829 .6946
00 .7051 .7037 .7109 .7167 .7124 -075 000 5 2
04 .6901 .6930 .7017 .7133 .7104
08 .6596 .6741 .6872 .7018 .6960
12 •6229 •5997 •6229 •6591 •6635
16 .4912 .5815 .6106 .6513 .6601
20 .4595 .5702 .6066 .6518 .6664
23 •4406 •5717 •6125 •6591 •6751
00 .7043 .7028 .7101 .7159 .7101 -030 000 5 2
04 .6931 .6945 .7048 .7135 .7106
C8 .6596 .6741 .6887 .7032 .6974
12 •6352 •6090 •6177 •6528 •6615
```

INDICATED TOTAL PRESSURE RATIOS FOR OAL TEST 289-19. H. = 2.00
PL/PL.

```
0.069 0.269 0.469 0.669 0.869
                                           ø E
                                      p_{R}
 16 .5715 .5584 .5947 .6354 .6470
 20 .4236 .5414 .5806 .6271 .6446
 23 .4030 .5381 .5831 .6325 .6499
 00 .7042 .7027 .7114 .7173 .7114 -085 000 5 2
 04 .6940 .6969 .7085 .7173 .7114
 08 .6611 .6785 .6930 .7075 .7075
 12 .6393 .6552 .6799 .6465 .6523
 16 .5773 .6063 .5744 .6180 .6310
 20 •4694 •5101 •5522 •6030 •6233
23 •4288 •5014 •5507 •6044 •6262
 20 .7056 .7027 .7114 .7187 .7114 -090 000 5 2
 04 .6935 .6979 .7080 .7167 .7124
 08 .6649 .6766 .6940 .7056 .7027
 12 .6461 .6606 .6751 .6954 .6954
 16 .5769 .6059 .6262 .6015 .6175
20 .5079 .4803 .5254 .5792 .6024
 23 .4723 .4665 .5188 .5769 .6001
 00 .7046 .7046 .7133 .7206 .7133 -095 000 5 2
 04 .6911 .6969 .7085 .7158 .7100
 08 .6564 .6765 .6911 .7056 .7013
 12 .6261 .6567 .6683 .6872 .6858
 16 .5243 .5999 .6189 .6509 .6029
 20 •5112 •5461 •5228 •5548 •5796
 23 44741 4726 4886 5498 5746
 00 .7032 .7076 .7120 .7150 .7091 -100 000 5 3
 00 .7022 .7081 .7125 .7155 .7081
 04 .6856 .7003 .7076 .7120 .7061
 08 .6665 .6841 .6959 .7018 .6989
 12 .5210 .6503 .6635 .6841 .6841
 16 •4093 •5960 •6135 •6456 •6529
 16 •4070 •5939 •6144 •6450 •6524
 20 •4283 •5469 •5601 •5762 •5630
 23 .3804 .5190 .5249 .5249 .5526
 00 •7049 •7064 •7137 •7195 •7122 -105 000 5 3
 04 •6786 •6991 •7049 •7137 •7093
 08 •6728 •6816 •6903 •7035 •7006
 12 •2984 •6485 •6616 •6806 •6806
 16 •3368 •5837 •6027 •6436 •6597
 20 .2715 .5377 .5494 .5802 .5875
 23 •2681 •5059 •5236 •5559 •5192
 00 .7060 .7045 .7118 .7191 .7133 -110 000 5
 04 •6645 •6968 •7056 •7174 •7115
 08 .6562 .6811 .6928 .7060 .7016
 12 •3498 •6489 •6591 •6811 •6811
16 •3361 •5780 •6159 •6407 •6480
 20 .3225 .5286 .5359 .5666 .5783
 23 •3733 •4993 •5111 •5433 •5521
00 .7065 .7036 .7123 .7197 .7138 -115 000 5
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INDICATED TOTAL PRESSURE HATIOS FOR OAL TEST 289-19 N = 2.00
            PÉ/Pt.o
     0.069 0.269 0.469 0.669 0.869
                                       Ø<sub>R</sub>
 04 .6459 .6973 .7061 .7179 .7120
 08 .5990 .6820 .6936 .7082 .7053
 12 .4542 .6494 .6596 .6831 .6846
 16 .3207 .5980 .6317 .6464 .6435
 20 .3334 .5239 .5341 .5605 .5693
 23 .3663 .4920 .5008 .5300 .5417
▶ 00 .7065 .7036 .7109 .7211 .7153 -120 000 5 3
  04 .6197 .6972 .7060 .7191 .7147
 08 .5056 .6826 .6957 .7118 .7074
 12 •4738 •6431 •6563 •6825 •6854
 16 .3361 .5882 .6340 .6397 .6426

√20 .3269 .5347 .5794 .6011 .5967

 23 .3446 .4990 .5150 .5310 .5281
 00 •7077 •7033 •7077 •7106 •7164 -125 000 5 3
 04 •5864 •6971 •7058 •7204 •7174
  08 .3950 .6830 .6960 .7106 .7077
  12 .5099 .6204 .6495 .6800 .6859
  16 .2659 .5077 .6140 .6271 .6359
20 .3242 .4320 .5878 .5922 .5922
  23 • 3264 • 3935 • 5351 • 5439 • 5380
  00 .7058 .7043 .7029 .7087 .7189 -130 000 5 3
  04 .5589 .6984 .7057 .7115 .7188
  08 .3242 .6839 .6971 .7145 .7116
  12 .4305 .5135 .6417 .6796 .6869
  16 .2516 .4921 .5139 .6072 .6305
  20 .2720 .3959 .5431 .5708 .5751
  23 .2428 .3988 .4964 .5227 .5197
  00 .7063 .7034 .7034 .7092 .7151 -135 000 5 3
  04 .5314 .7005 .7034 .7092 .7194
  08 .2785 .6850 .6981 .7113 .7128
  12 •3508 •3991 •6348 •6787 •6889
  16 .3222 .5443 .4479 .5720 .6202
  20 .2581 .4409 .4716 .5227 .5549
  23 .2974 .4990 .3836 .4683 .4858
  00 .7084 .7084 .7084 .7055 .7025 -150 000 5 3
  04 .5034 .7070 .7070 .7041 .7070
  08 .3347 .6860 .6977 .7065 .7094
  12 .3090 .3295 .6523 .6846 .7022
  16 .5576 .1928 .1737 .5444 .6425
  20 .5737 .4873 .2060 .3144 .3818
  23 .5151 .3525 .2118 .2734 .3085
```

INDICATED	TOTAL	PRESSURE	RATIOS	FOR	OAL	TEST	289-19	M _o =	= 2.00
	Pé/F	وريا					_		
								d	

Υ _ξ Ω	1.069	1.269	1.469	1.669	$p_{ m R}$	ø.	Rake	Run
00 04 08 12 16	•7015 •7201 •7497 •7826	•6990 •7030 •7245	•6980 •6976 •7044 •7259 •7526 •7841 •6040	•6976 •7059 •7274 •7555 •7855	030	000	5	1 .
04 08 12	•7372 •7280 •7566	.7019 .7086 .7309 .7589 .7906	•7019 •7101 •7324 •7595	.7034 .7130 .7339 .7524	015	000	5	1
00 04 08 12 16 20 23	₽7909	.7014 .7119 .7320	• 7909	•7378 •7647	000	000	5	1
04	•7048 •7028 •7067 •7250 •7542 •7836 •8066	7496729475717851	.6999 .7110 .7308 .7600		- 015	000	5	1
00 04 08 12 16 20 23	.6946 .6941 .6965 .7135 .7377 .7659	.6898 .6950 .7150 .7406 .7746	•6956 •6979 •7193 •7508 •7775	.7004 .7000 .7067 .7251 .7522 .7804 .3051	- 030	000	5	1
04 08 12 16	.6980 .6980 .7111 .7339	•7077 •7053 •7096 •7257 •7484 •7728 •7929	•7024 •7096 •7242 •7484 •7728	•7082 •7242 •7469	-040	000	5	1
04 08 12	7063706371517355	.7049 .7019 .7034 .7165 .7384 .7626	•6976 •7019 •7165 •7384	•7384	- 745	000	5	1

If DIG ITED TOTAL PRESSURE RATIOS FOR GAL TEST 289-19 $u_0 = 2.00$ PE/Pe.0

	•	TE/ TE,	,5		9		
a _j y	1.069	1.269	1.469	1.669	$\mathbf{p}_{\mathbf{R}}$	g 2	E C
23	•7772.	• 7815	•7801	•7772			
12 16	•7037 •7090 •7256 •7503	.7002 .6993 .7105 .7285	.6958 .6993 .7105 .7299	.6964 .6944 .6993 .7120 .7314 .7547	- 050	000 5	2
04	•7018 •7163	.6968 .6960 .7132 .7207 .7440	•6953 •6960 •7076	•6989 •7120 •7280 •7483	- 055	000 5	2
00 04 08 12 16 20 23	.6989 .6941 .6945 .7062	.6945 .6941 .6960 .7121 .7359	.6955 .7032 .7179 .7403	•6960 •6984 •7061 •7208	- 060	000 5	2
00 04 08 12 16 20 23	.7014 .6897 .6844 .6956	.6976 .6927 .6902 .7058	.6989 .6970 .6956 .596 .7116 .7312 .7456	•6970 •6985 •7004 •7146 •7312	- 065	000 5	2
00 08 12 16 20 23	•6844 •6805 •6854 •6990	.7014 .6902 .6878 .6970 .7151	.6994 .7000 .6931 .6937 .7043 .7209	•7000 •6946 •6981 •7073 •7209	- 079	000 5	2
00 C4 08 12 16 20 23	•6858 •6751 •6761 •6839 •6853	.7051 .6988 .6887 .6892 .7013	.7051 .6988 .6930 .6896 .6965	•7051 •6988 •6945 •6925 •6994 •7101 •7188	~ 075	000 5	2
00 04 08	• 7048	•7043 •7019 •6901	.7043 .7019 .6916	•7028 •7019 •6945	-080	000 5	2

IM	CATED	TOTAL P		HATIOS	FOR	OAL	TRST	289-1	9	N = 2.0	o
		PE/PL	,0							0	
a _i y	1.069		1.469	1.669			$\phi_{_{ m I\!R}}$	ø	teke	5	
12 16 20	•6707	•6804 •6867	•6940	•6906 •6969				·	~		
12	•7056 •7085	•7056 •7056 •6944 •6756	•7056 •693′	•7042 •7042 •5959 •6857			-085	000	5	2	
20 23		.6727 .6785									
04	70956984663564366358	•7071 •7080 •6969 •6707 •6582 •6562	.7051 .6940 .6780 .6663 .6678	•7051 •6940 •6809 •6727 •6707			-090	000	5	2	
04	7085699865816334	•6984 •6654 •6509 •6392	.7056 .6969 .6712 .6596	•7056 •6940 •6770 •6654 •6567		,	- 095	000	5	2	
00 04 08 12 16 16 20 23	.7067 .7076 .7018 .6870 .6251 .6261	•7≎76	•7067 •7061 •7003 •6709 •6529 •6524 •6416	•7052 •7047 •6989 •6753 •6587 •6582			-100	000	.5	3	
00 04 08 12 16 20 23	•7079 •7020 •6879 •6144	•6893 •5319 •6050	.7079 .7020 .5893 .6436 .6197	•7049 •6991 •6747 •6494		•	-105	000	5	3	
00 08 12 16 27 23	773068856742	•6914 •6844 •5885	.7030 .6929 .6334	•6393 •6104		•	-110	000	5	3	

١.

INDICATED TOTAL PRESCURE RATIOS FOR GAL TEST 289-19 No = 2.00 PE/P4.0

		,	,.				
a ₁ y	1.069	1.269	1.469	1,669	$p_{\hat{\mathbf{R}}}$	à S	
00 04 08 12 16 20 23	• 7065 • 7091 • 7053 • 6904 • 6699 • 6015 • 5622	.7065 .7091 .7053 .6919 .6772 .6030	•6934 •6816	•7076 •6995 •6904 •6347	-115	000 5	3
∨ 00 04 08 12 16 ∨29 23	•7060 •6913	•7065 •7089 •7060 •6927 •6741 •6155 •5747	•7074 •7030 •6927 •6770 •6256	•7045 •7001 •6898 •6755	-120	000 5	3
00 04 08 12 16 20 23	•7077 •7087 •7033 •6902 •6577 •6213 •5439	•7077 •7087 •7048 •6931 •6738 •6388 •5614	.7058 .7019 .6931	• 7019 • 7029 • 7019 • 6902 • 6767 • 6563 • 5687	-125	000 5	3
00 04 08 12 16 20 23	•7087 •7101 •7058 •6912 •6553 •6043 •5314	.7072 .7043 .6941	•6801		-130	000 5	3
00 04 08 12 16 20 23	•7121 •7121 •7084 •5948 •6553 •5914 •5092	.7063 .7063 .7055 .6948 .6713 .6236	•7005 •7034 •7040 •6948 •6816 •6528 •5998	.6990 .7019 .7025 .6977 .6933 .6616	-1 35	000 5	3
00 04 08 12 16 20 23	•7055 •7099 •7167 •7080 •6880 •5863 •4404	•7173 •7138 •7051	•7110 •6938	•7084 •7099 •7109 •7080 •6053 •6601	-150	000 5	3

INDICATED TOTAL PRESSURE RATIOS FOR OAL TEST 289-19 M_o = 2.00 Pt/Pt_o

```
y 2.069 2.269 2.469 2.669 2.869
ai
                                     p_{\mathbf{p}}
                                          000 5
00 •6951 •6907 •6878 •6907 •6907
                                     030
04 .6976 .6976 .6932 .6932 .6903
08 .7073 .7088 .7088 .7088 .7088
12 • 7303 • 7303 • 7332 • 7347 • 7332
16 • 7599 • 7570 • 7599 • 7613 • 7628
20 .7885 .7855 .7885 .7885 .7929
23 .8098 .8054 .8084 .8069 .7104
00 •7023 •6994 •6979 •6950 •6936 015 000 5 1
04 .7034 .7019 .7019 .7019 .7005
08 •7159 •7159 •7173 •7202 •7188
12 • 7368 • 7382 • 7397 • 7426 • 7455
16 .7653 .7653 .7653 .7667 .7755
20 .7920 .7906 .7920 .7949 .7135
23 •8106 •8092 •8077 •7061 •7076
00 •6984 •6970 •6941 •6926 •6897 000 000 5 1
04 •7029 •7014 •6985 •7000 •7000
08 •7177 •7177 •7177 •7207 •7207
12 •7408 •7408 •7468 •7437 •7495
16 • 7647 • 7662 • 7647 • 7576 • 7764
20 .7938 .7909 .7880 .7967 .. 7081
23 •8112 •8083 •7735 •7037 •7023
00 •6990 •6960 •6917 •6902 •6888 -015 000 5
04 • 7014 • 7014 • 6970 • 6984 • 6970
08 •7125 •7125 •7125 •7168 •7154
12 • 7352 • 7352 • 7352 • 7395 • 7410
16 .7629 .7629 .7615 .7629 .7717
20 • 7894 • 7865 • 7836 • 7865 • 7952
23 .8065 .8051 .8022 .6990 .6946
00 •7091 •7048 •7004 •6960 •6931 -030 000 5 1
04 .7102 .7087 .7043 .7043 .7014
08 .711C .7183 .7183 .7197 .7183
12 •7324 •7382 •7368 •7397 •7368
16 • 7624 • 7624 • 7595 • 7624 • 7595
20 •7891 •7862 •7848 •7848 •7818
23 .8066 .8037 .8008 .8008 .6917
00 •6975 •6960 •6960 •6931 •6931 -040 000 5 1
04 .6980 .6980 .6966 .6995 .6995
08 .7067 .7067 .7096 .7126 .7126
12 •7242 •7242 •7271 •7315 •7315
16 •7469 •7469 •7484 •7523 •7513
20 •7684 •7713 •7713 •7742 •7728
23 .7841 .7870 .7856 .7900 .7870
00 •6976 •6961 •6961 •6947 •6917 •045 000 5 1
04 •6976 •6976 •6961 •5990 •6990
08 .7034 .7063 .7078 .7107 .7121
12 •7194 •7223 •7238 •7282 •7282
16 •7413 •7442 •7457 •7500 •7471
20 •7626 •7655 •7655 •7699 •7684
```

APPENDIX B (CONTINUED) . INDICATED TOTAL PRESSURE RATIOS FOR CAL TEST 289-19 u_n = 2.00

Pi/Pto 15 2.069 2.269 2.469 2.669 2.369 Ø, 23 .7772 .7815 .7786 .7830 .7815 00 .6964 .6949 .6949 .6935 .6906 -050 000 5 04 •6958 •6958 •6958 •6973 •6958 08 •7022 •7037 •7051 •7080 •7095 12 •7163 •7192 •7207 •7251 •7251 16 .7343 .7401 .7401 .7445 .7445 20 .7561 .7619 .7605 .7648 .7648 23 • 7693 • 7765 • 7750 • 7779 • 7765 00 •6968 •6953 •6939 •6924 •6924 -055 000 5 04 •6968 •6968 •6982 •6968 08 .7018 .7032 .7047 .7076 .7076 12 .7134 .7163 .7192 .7221 .7236 16 .7294 .7352 .7352 .7411 .7425 20 •7483 •7556 •7556 •7600 •7585 23 .7603 .7690 .7661 .7690 .7690 00 •6984 •6970 •6955 •6941 •6941 -060 000 5 04 •6960 •6960 •6960 •6960 •6960 08 .6999 .7013 .7013 .7057 .7072 12 .7090 .7149 .7149 .7207 .7207 16 .7237 .7296 .7296 .7354 .7368 20 •7418 •7476 •7476 •7520 •7534 23 • 7520 • 7607 • 7593 • 7651 • 7636 00 •6960 •6945 •6930 •6930 •6916 •065 000 5 04 •6970 •6970 •6956 •5970 •6956 08 .7000 .7014 .7014 .7043 .7043 12 • 7033 • 7062 • 7091 • 7135 • 7164 16 •7160 •7219 •7233 •7292 •7306 20 •7297 •7399 •7399 •7458 •7472 23 • 7398 • 7514 • 7500 • 7543 • 7529 00 •6965 •6950 •6936 •6921 •6906 -070 000 5 04 •7000 •6970 •6970 •6970 •6956 08 •6960 •6975 •6989 •7019 •7019 12 •6995 •7039 •7068 •7112 •7127 16 .7087 .7160 .7189 .7248 .7262 20 •7195 •7297 •7297 •7370 •7355 23 •7282 •7414 •7370 •7443 •7443 00 •7022 •7008 •6964 •6964 •6949 -075 000 5 04 •6973 •6959 •6930 •6973 •6959 08 •6974 •6974 •6960 •7018 •7032 12 •6954 •7012 •6997 •7070 •7099 16 •7008 •7096 •7096 •7183 •7198 20 • 7086 • 7203 • 7174 • 7261 • 7276 23 •7159 •7305 •7247 •7334 •7334 00 •7013 •6984 •6955 •6984 •6970 -080 000 5 04 •7004 •6989 •6960 •6989 •6975 08 •6960 •6974 •6945 •7003 •7003 12 •6951 •6994 •6994 •7053 •7067

```
IMDICATED TOTAL PRESSURE RATIOS FOR OAL TEST 289-19 Mg = 2.00
           Pé/Pero
                                         5 2
y 2.069 2.269 2.469 2.669 2.869
                                   PR
16 •6935 •7022 •7008 •7109 •7095
20 •6969 •7085 •7056 •7143 •7173
23 .7022 .7167 .7138 .7196 .7211
00 .7027 .6998 .6969 .6984 .6969 -085 000 5 2
04 .7027 .7027 .6998 .6998 .6984
08 .6973 .6988 .6959 .6973 .6988
12 .6886 .6930 .5930 .6988 .7002
16 .6848 .6935 .6935 .7008 .7022
20 .6828 .6959 .6944 .7046 .7061
23 .6357 .7017 .6973 .7046 .7046
00 .7056 .7042 .7027 .7027 .6984 -090 000 5 2
04 .7051 .7037 .6993 .6993 .6993
08 •6954 •6954 •6940 •6969 •6969
12 •6838 •5896 •6896 •6954 •6954
16 •6756 •6357 •6857 •6930 •6959
20 •6693 •6838 •6795 •6911 •6940
23 .6698 .6872 .6799 .6915 .6930
00 .7075 .7031 .6988 .6988 .6973 -095 000 5
04 • 7042 • 6998 • 6969 • 6984 • 6969
08 •6940 •6940 •6896 •6940 •6940
12 •6785 •6843 •6829 •6916 •6916
16 •6654 •6770 •6756 •6843 •6872
20 •6567 •6712 •6683 •6800 •6829
23 .6518 .6722 .6664 .6766 .6766
00 .7047 .7032 .7003 .7003 .6973 -100 000 5
00 •7037 •7008 •6978 •6978 •6964
04 • 7047 • 7032 • 7003 • 7003 • 6973
08 .6959 .6959 .6930 .6959 .6944
12 •6768 •6826 •6826 •6885 •6885
16 .5602 .6689 .6689 .6762 .6806
16 .6597 .6699 .6699 .6772 .6816
20 .6450 .6626 .6596 .6714 .6728
23 .6358 .6577 .6533 .6636 .6636
00 •7049 •7020 •6976 •6991 •6962 -105 000 5 3
04 .7049 .7020 .6962 .6991 .6962
08 .6962 .6947 .6903 .6918 .6874
12 .6733 .6777 .6733 .6791 .6806
16 •6494 •6597 •6582 •6684 •6713
20 .6255 .6445 .6416 .6533 .6562
23 •6131 •6366 •6337 •6440 •6454
00 .7030 .7001 .6957 .6972 .6972 -110 000 5 3
04 .7056 .7027 .6983 .6968 .6939
08 •6972 •6943 •6870 •6884 •6855
12 .6738 .6738 .6709 .6767 .6767
16 •6422 •6538 •6538 •6626 •6655
20 .6119 .6324 .6324 .6441 .6470
23 •5946 •6196 •6181 •6284 •6298
00 •7036 •7006 •6962 •6962 •6918 -115 000 5 3
```

INDICATED TOTAL PRESSURE RATICS FOR OAL TEST 289-19 $\mu_0 = 2.00$

```
de sa mi
   2.069 2.269 2.469 2.669 2.369
 04 .7047 .7003 .5959 .6944 .6914
 08 •6980 •6936 •6878 •6893 •6864
 12 •6846 •6787 •6728 •6758 •6758
 16 .6376 .6494 .6508 .6582 .6611
 20 •6045 •6250 •6250 •6367 •6396
 23 •5797 •6061 •6046 •6177 •6236
1 100 • 7006 • 6977 • 6948 • 6948 • 6918 −120 000 5 3
 04 .7016 .6987 .6943 .6943 .6913
 08 •6987 •6957 •6913 •6913 •6870
 12 •6869 •6854 •6767 •6767 •6767
 16 •6641 •6512 •6469 •6555 •6569
20 .5982 .6184 .6198 .6328 .6400
 23 •5631 •5922 •5951 •6097 •6126
 00 •6990 •6960 •6917 •6931 •6902 -125 000 5 3
 04 • 7029 • 6971 • 6941 • 6941 • 6912
 08 •6975 •6960 •6917 •6931 •6902
 12 •6888 •6902 •6844 •6844 •6815
 16 •6738 •6796 •6592 •6621 •6650
 20 .5922 .6170 .6170 .6301 .6330
 23 •5526 •5818 •5847 •5993 •6052
 00 .7000 .6971 .6912 .6941 .6912 -130 000 5 3
 04 •7014 •6955 •6926 •6955 •6926
 08 .7000 .6971 .6941 .6956 .6956
 12 •6912 •6941 •6898 •6941 •6883
 16 .6786 .6888 .6815 .6830 .6742
20 •6670 •6699 •6597 •6349 •6393
 23 •5869 •5722 •5780 •5926 •5985
 00 •6976 •6947 •6917 •6932 •6917 -135 000 5 3
 04 •7005 •6976 •6947 •6961 •6976
 08 •7011 •6996 •6996 •7040 •6996
 12 •6992 •7006 •6948 •6977 •6948
 16 •6903 •6933 •6859 •6903 •6874
 29 •6631 •6762 •6762 •6762 •6718
 23 •6202 •6465 •6480 •6524 •6085
 00 •7055 •6996 •6938 •6996 •6967 -150 000 5 3
 04 .7070 .7070 .7011 .7041 .7011
 08 •7123 •7065 •7036 •7065 •7036
 12 •7066 •7066 •7007 •7051 •7051
 16 .6982 .6997 .6982 .7026 .6997
 20 .6645 .6777 .6748 .6836 .6850
 23 •6220 •6425 •6455 •6572 •6601
```

INDICATED TOTA	l pressure	RATIOS	FOR	OAL TEST	289	- 19	M _o = 2.00
y 3.069 3.269	3.469			g_{R}	ø	Rake	Hank Hank
00 .6849 .6776 04 .6932 .6990 08 .7103 .7249 12 .7420 .7508 16 .7730 .7818 20 .7094 .7079 23 .7045 .7030	.7092 .7380 .7610 .7891 .7094			030	000	5	1
00 .6878 .6820 04 .6990 .7078 08 .7261 .7362 12 .7557 .7659 16 .7856 .7958 20 .7091 .7106 23 .7032 .7047	•7180 •7449 •7746 •7130 •7106			015	000	5	1
00 .6854 .6810 04 .6985 .7073 08 .7294 .7395 12 .7582 .7684 16 .7880 .7430 20 .7067 .7081 23 .6994 .7023	•7174 •7497 •7786 •7125 •7067			000	000	5	1
00 .6830 .6757 04 .6955 .7028 08 .7226 .7328 12 .7526 .7627 16 .7804 .7920 20 .6994 .7023 23 .6931 .6975	•7115 •7415 •7714 •7106 •7037			-015	000	5	1
00 .6859 .6800 04 .6971 .7029 08 .7212 .7299 12 .7455 .7557 16 .7682 .7798 20 .7906 .7019 23 .6888 .6931	•7131 •7386 •7659 •7885 •7048			-030	000	5	1
00 .6888 .6830 04 .6966 .7009 08 .7155 .7257 12 .7373 .7475 16 .7571 .7702 20 .7786 .7903 23 .7068 .6908	•7111 •7344 •7577 •7789 •7014			-040	000	5	1
00 .6888 .6830 04 .6961 .6990 08 .7121 .7223 12 .7311 .7413 16 .7515 .7632 20 .7699 .7815	.7092 .7311 .7530 .7734			- 045	000	5	1

```
INDICATED TOTAL PRESSURE RATIOS FOR OAL TEST 289-19 No = 2.00
       FE/PLIO
3.069 3.269 3.469
 23 .7815 .6898 .6912
 00 •6862 •6804 •6877
                                     -050 000 5
 04 •6929 •6958 •7060
 08 .7095 .7182 .7284
 12 •7265 •7367 •7483
 16 .7460 .7547 .7634
 20 • 7677 • 7749 • 7836
 23 .7793 .7822 .6870
00 .6881 .6823 .6895
                                     -055 000 5
04 •6968 •6982 •7069
08 .7090 .7149 .7265
12 .7251 .7323 .7425
16 .7440 .7498 .7600
20 .7629 .7658 .7745
23 •7748 •7777 •7821
00 •6911 •6853 •6926
                                     -060 000 5 2
04 •6930 •6960 •7047
08 .7072 .7115 .7232
12 • 7221 • 7265 • 7367
16 .7398 .7441 .7543
20 .7593 .7622 .7666
23 • 7709 • 7739 • 7724
00 ,6887 .6829 .6901
                                    -065 000 5 2
04 •6941 •6941 •7043
08 .7058 .7073 .7175
12 •7193 •7208 •7296
16 • 7365 • 7379 • 7423
20 • 7531 • 7560 • 7560
23 •7616 •7660 •7660
00 .6877 .6834 .6921
                                    -070 000 5 2
04 •6941 •6941 •7029
08 •7048 •7048 •7150
12 •7171 •7185 •7244
16 .7321 .7335 .7335
20 •7443 •7472 •7487
23 •7531 •7560 •7575
00 .6906 .6848 .6935
04 .6959 .6930 .7017
                                    -075 000 5
                                                 2
08 •7032 •7032 •7090
12 •7142 •7157 •7157
16 •7256 •7285 •7299
20 • 7363 • 7392 • 7407
23 • 7436 • 7480 • 7480
00 •6926 •6882 •6955
                                    -080 000 5 2
04 •6960 •6902 •6989
98 .7003 .7003 .7032
12 •7111 •7140 •7140
```

INDICATED TOTAL FRESSURE RATIOS FOR OAL TEST 289-19 M. = 2.00

	P.	Pt.0	. 1100000.01	2013 200 1011	2,3	•		M 2.
	_	•	2 4/2		4	Ŕ	å	#
1/2	3.059	3.269	3.409		$\nu_{\mathbf{R}}$	ĸ	PĀ.	a <u>i</u>
a ₁ /			700-					
	• 7] 96	•7225	◆ /225 7310					
20 23		.7303 .7356						
D	• 1521	• 1)) 0	• 1326					
00	.6925	•6867	∙694 0		-085	000	5	2
0.4		•6896						
0.8		•7002						
12		•7075						
		•7138 •7191						
		.7235						
	• , 1 > 1							
0.0	•6940	•6832	• 6969		-090	000	5	2
		•69∂6						
		•6969 7049						
		•7041 7075						
16 20		.7075 .7085						
23		.7104						
_ ,	• • • •	• , 2 .						
		• 6872			-095	000	5	2
		•68R2						
		•6969						
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		•6851			-110	000	כ	3
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16. Abstract					
The Bumblebee Program, initiated in 1945 by the U.S. Navy Bureau of Ordinance, was designed to provide a supersonic-guided missile. The Aerodynamic Program included a fundamental research effort in supersonic aerodynamics as well as a design task in developing both vehicles and prototypes of tactical missiles. A series of four reports were prepared in order to facilitate dissemination of a large amount of fundamental aerodynamic missile data, which has been stored for a number of years at the Applied Physics Laboratory. This report provides data that supplements the M = 2.0 flow field data given in Part II. The enclosed data package (Appendix A) describes the Mach number effect by means of pressure fields only, at M = 1.5 and 2.0, and at angles of attack up to 23° at a mid-body station where a wing might be located.					
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